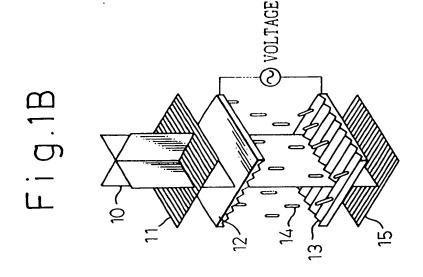
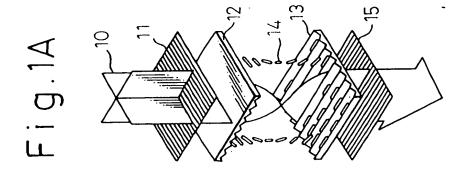
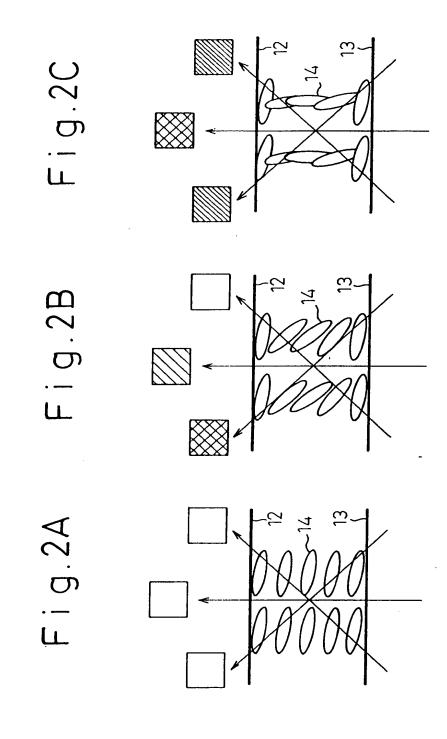
1/246





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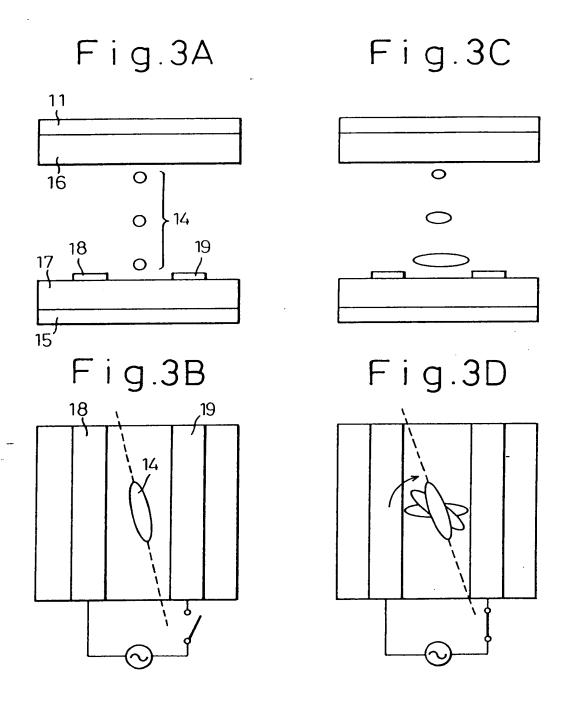




Fig.4

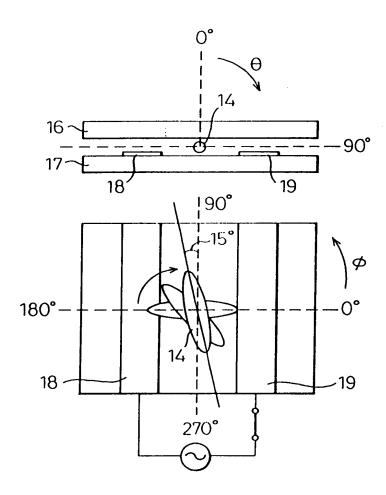
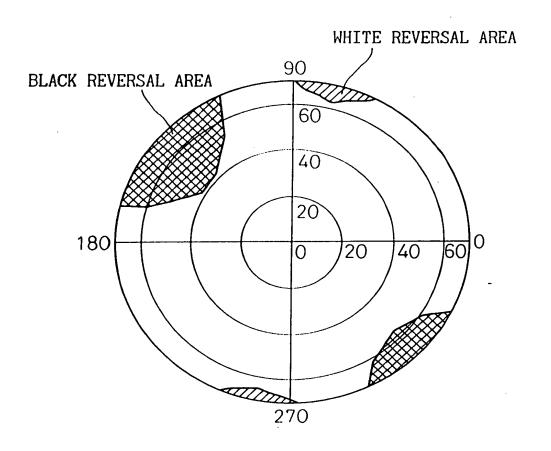
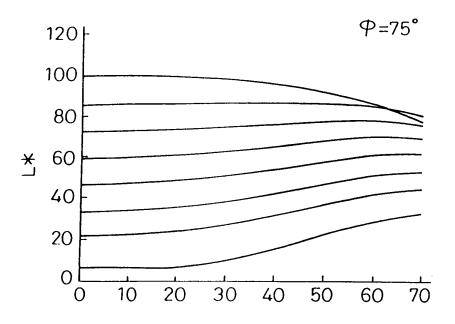
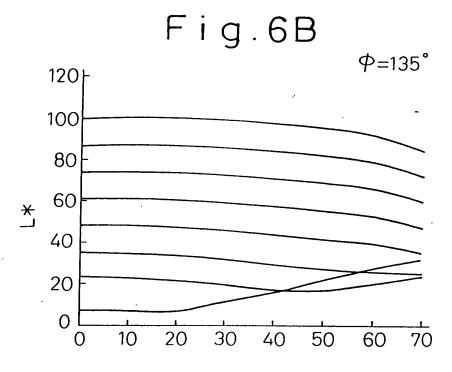


Fig.5

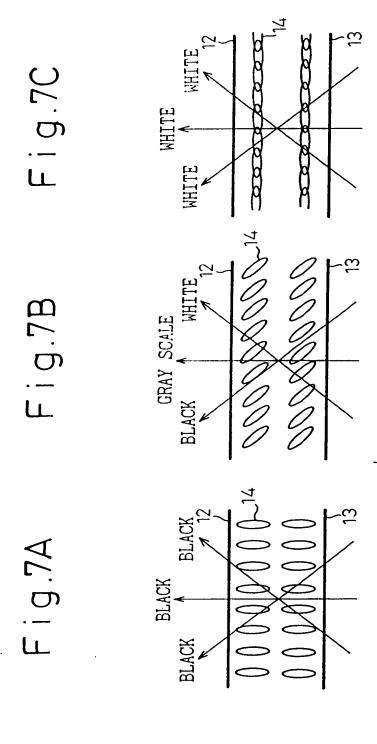


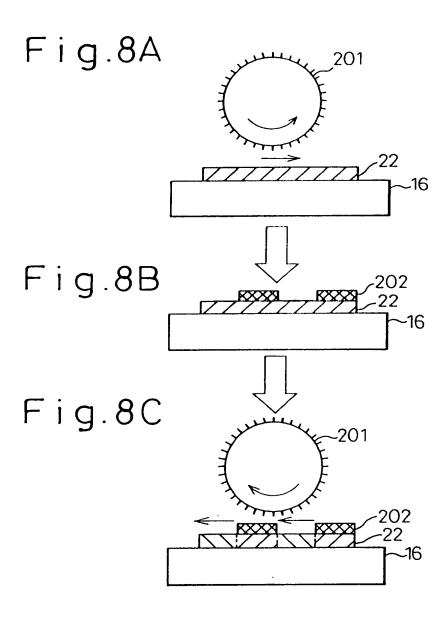
⁶/₂₄₆ Fig.6A

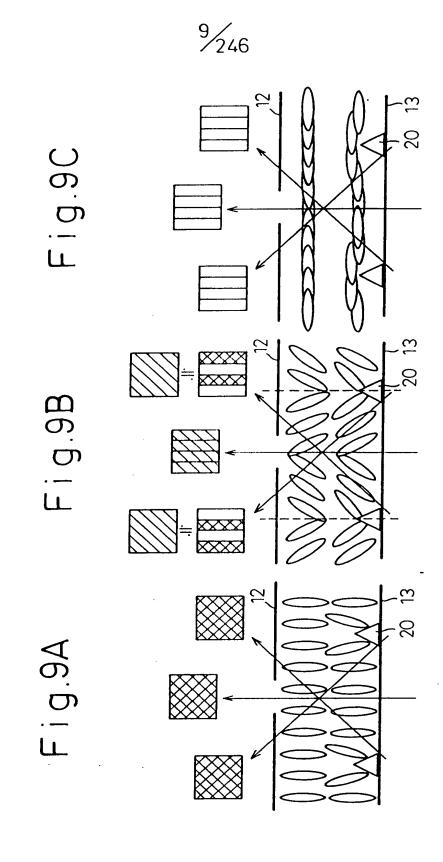




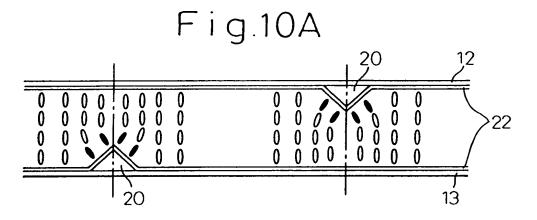
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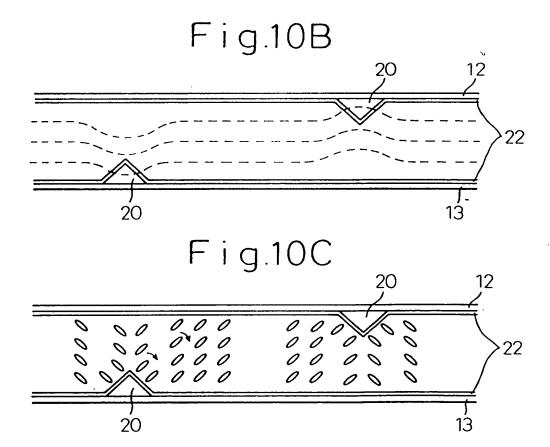


Fig.11A

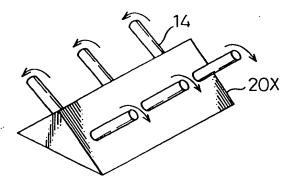


Fig.11B

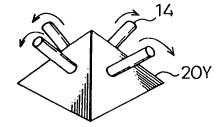
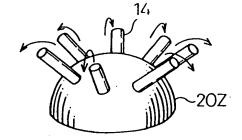


Fig.11C



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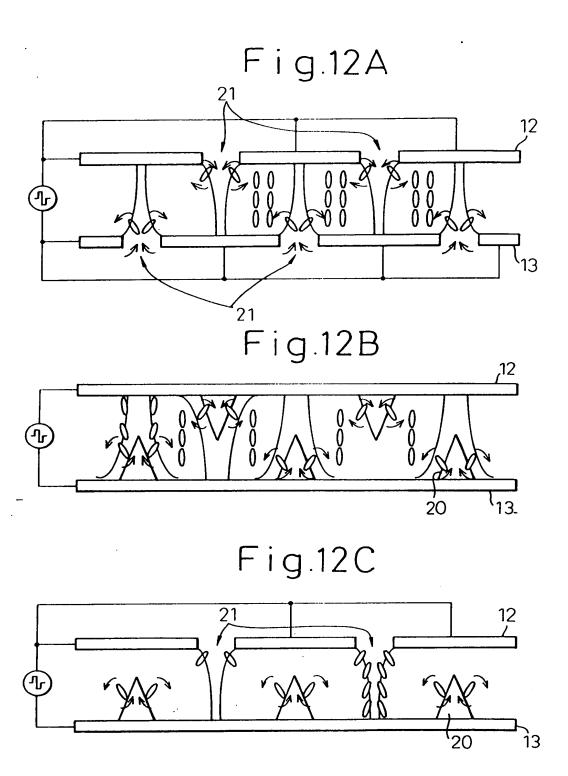




Fig.13

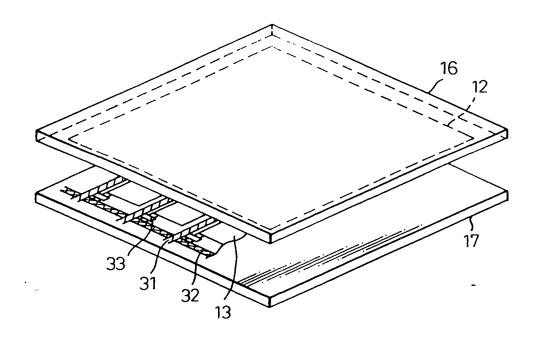




Fig.14A

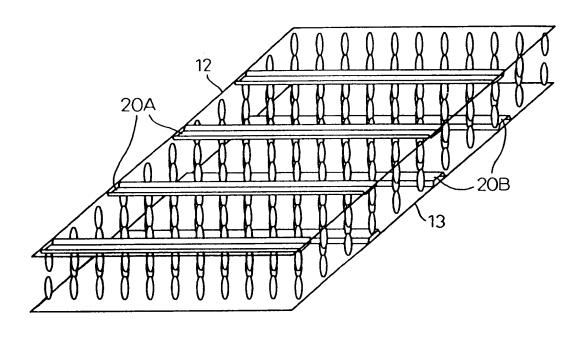


Fig.14B

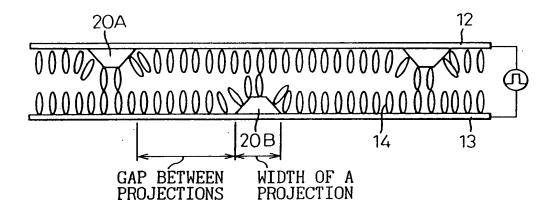




Fig.15

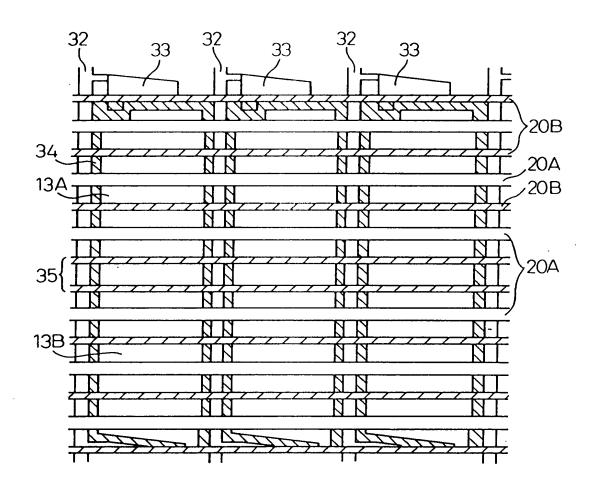
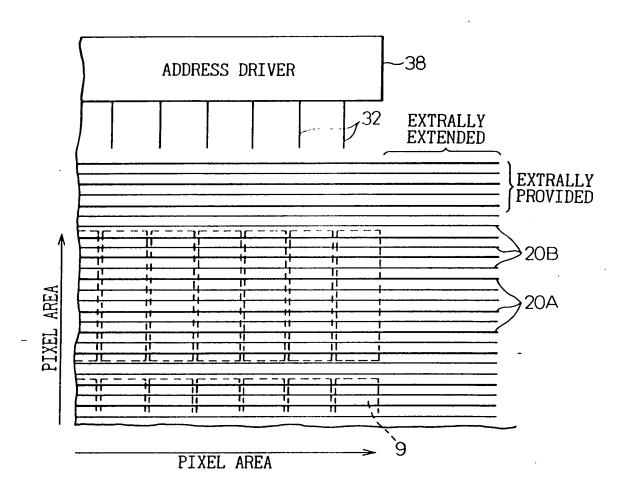


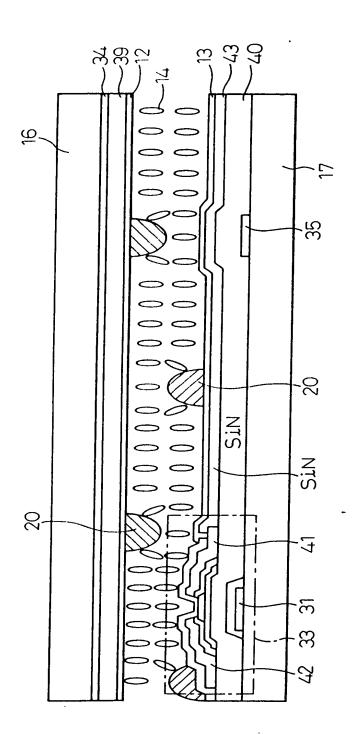


Fig.16





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F i g.17



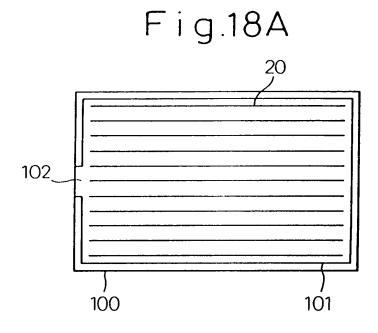
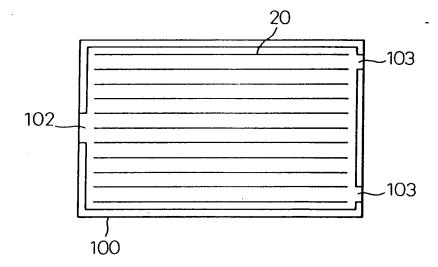
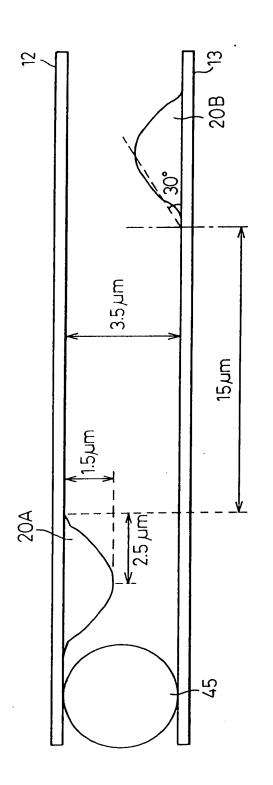


Fig.18B





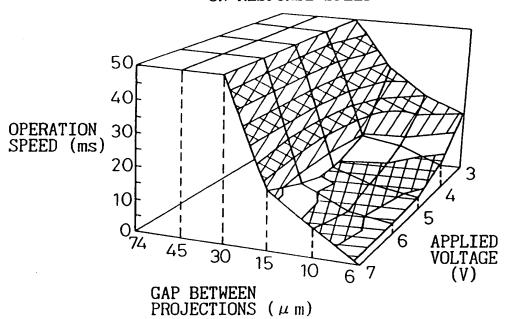
19₂₄₆



F i g .19

Fig.20A

ON RESPONSE SPEED



OPERATION SPEED (ms) 20

GAP BETWEEN PROJECTIONS (μ m)



Fig. 21

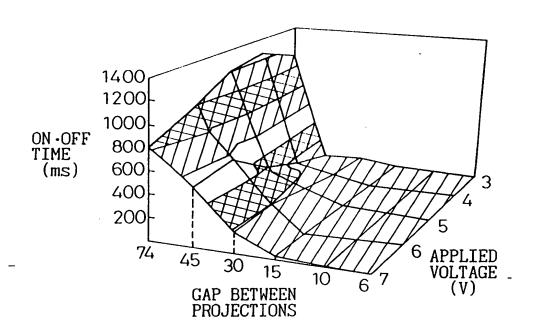
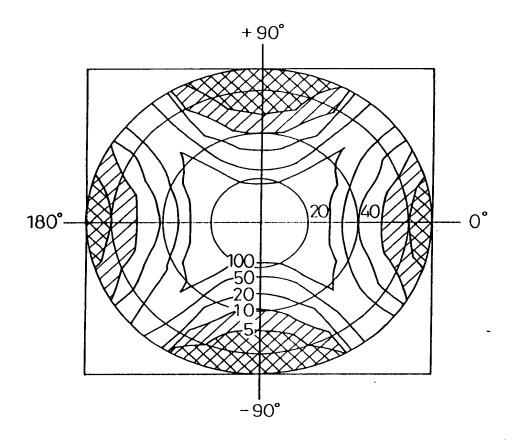
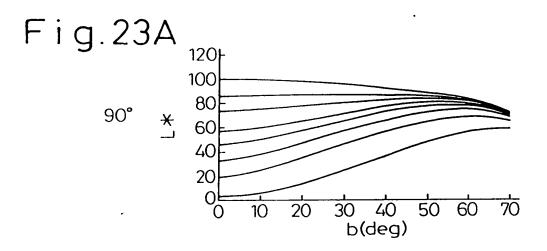


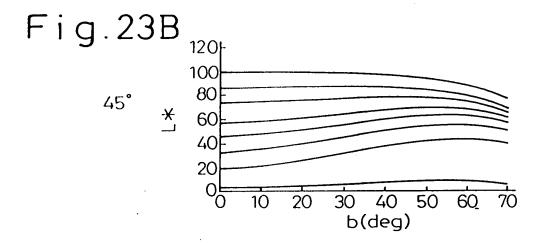


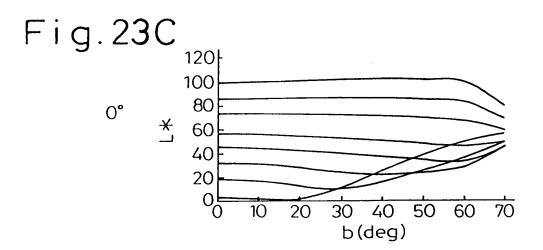
Fig. 22

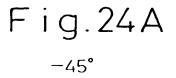












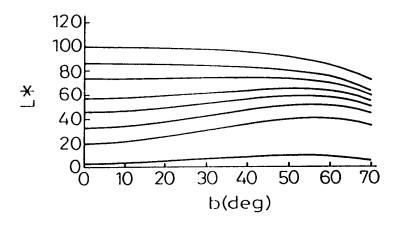


Fig.24B

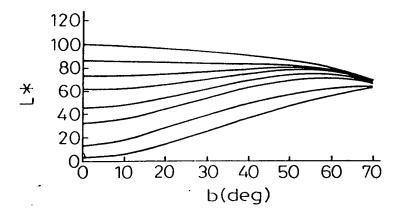




Fig.25

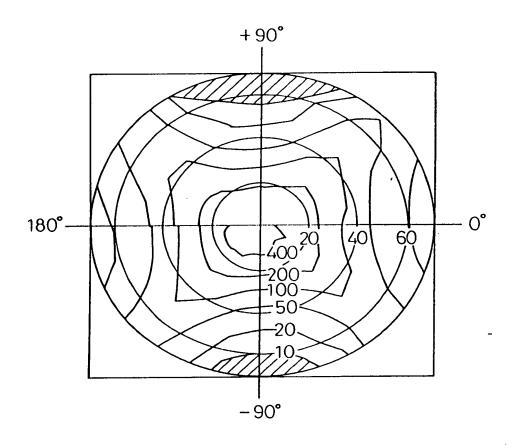




Fig.26A

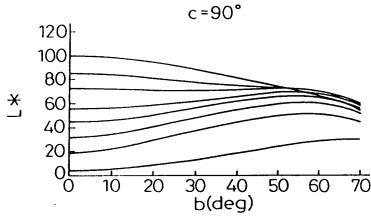


Fig.26B

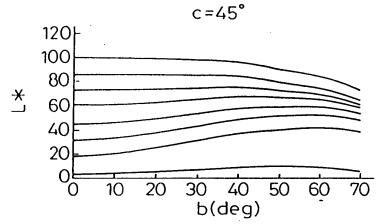


Fig.26C

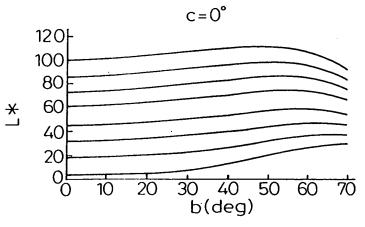
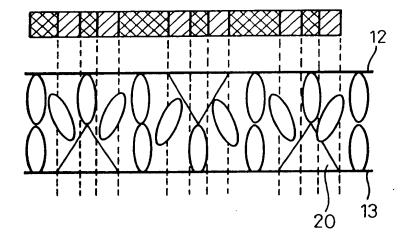
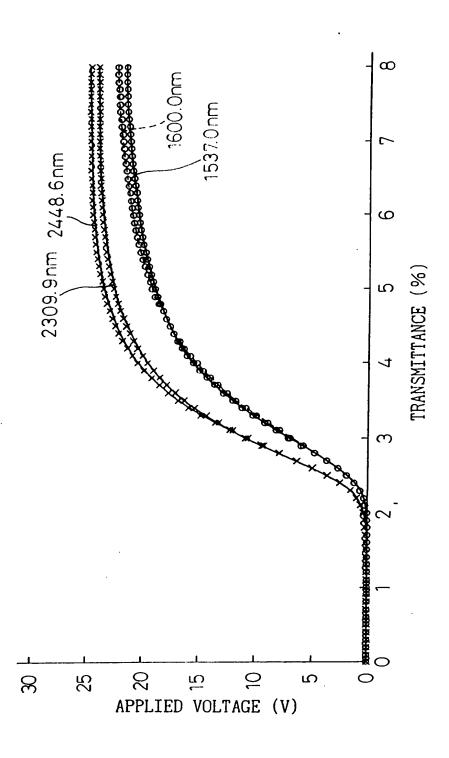




Fig. 27

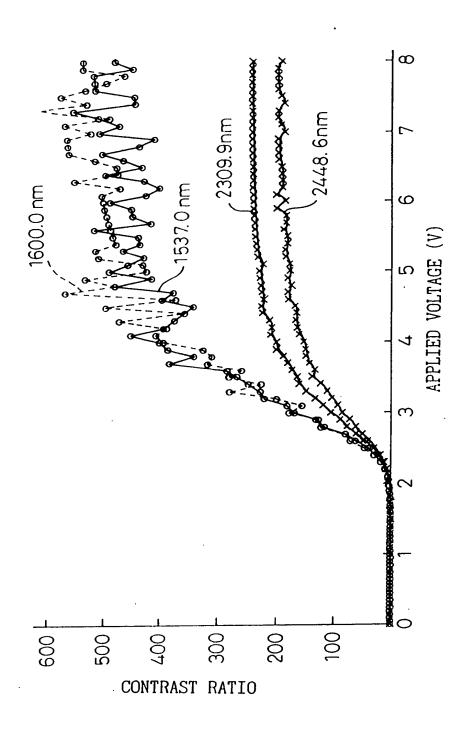


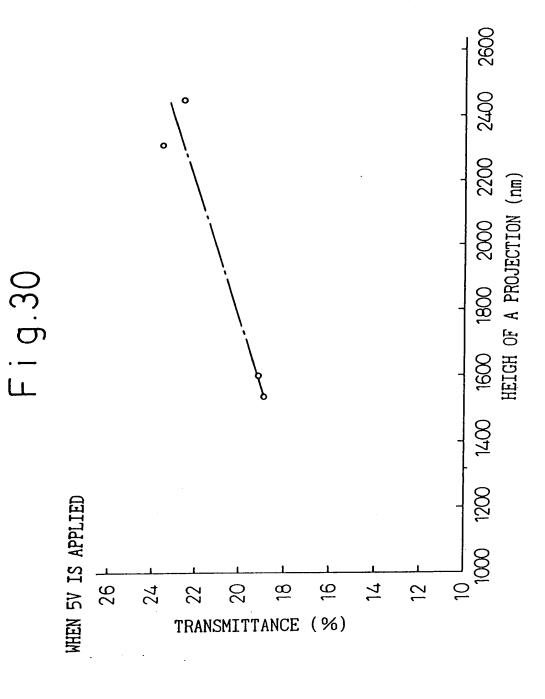
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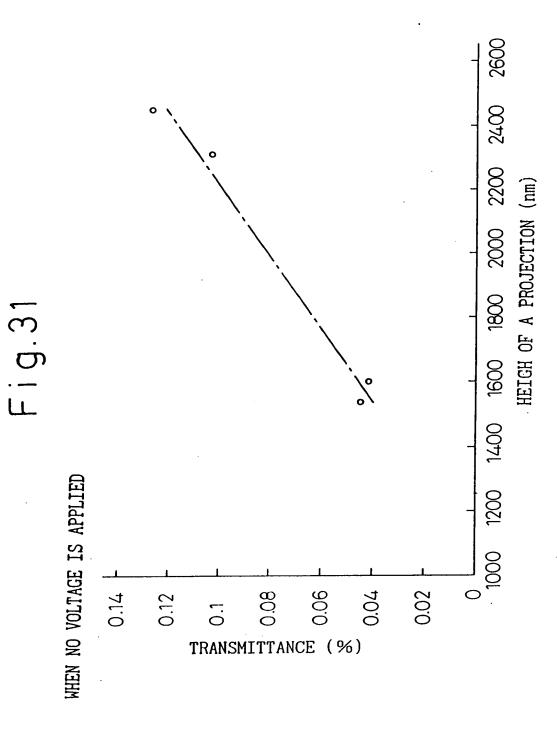
F i g.28

²⁹/₂₄₆











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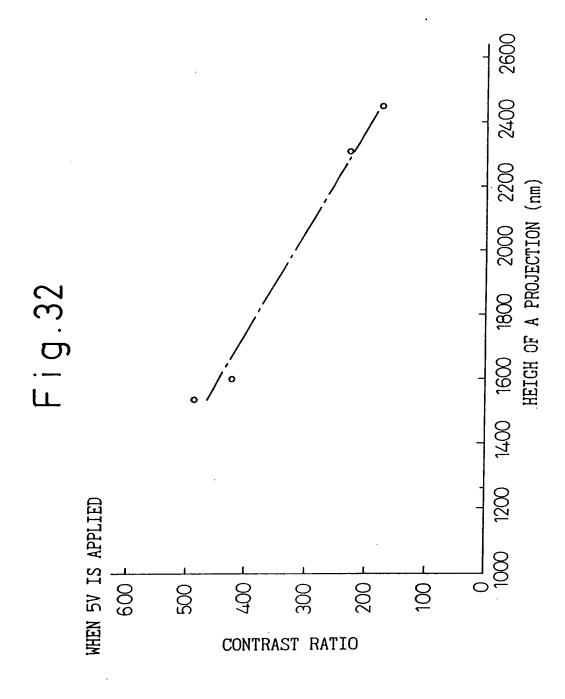




Fig.33

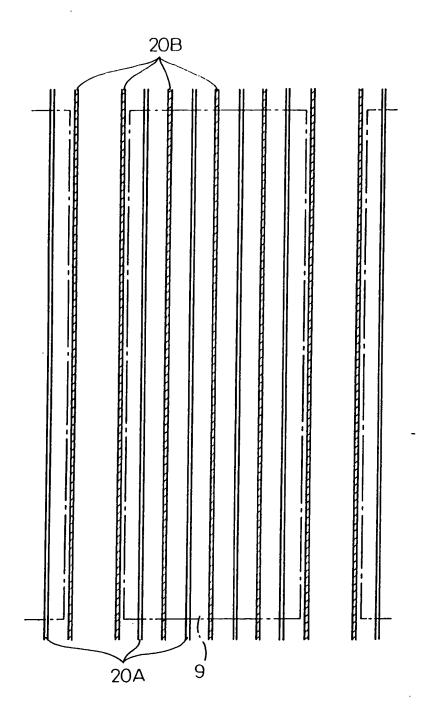




Fig.34

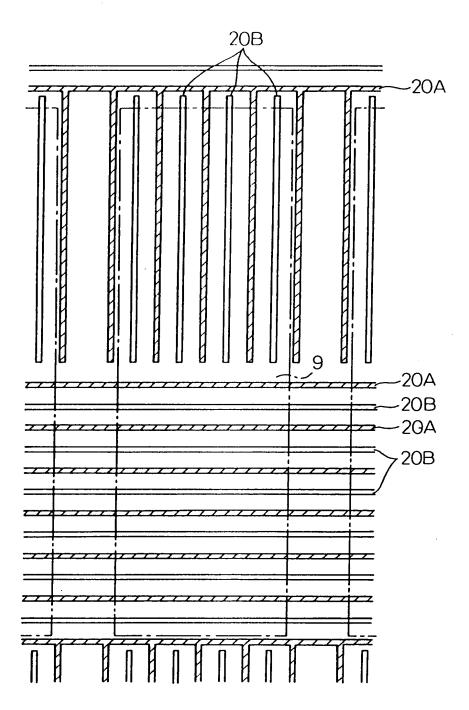




Fig.35

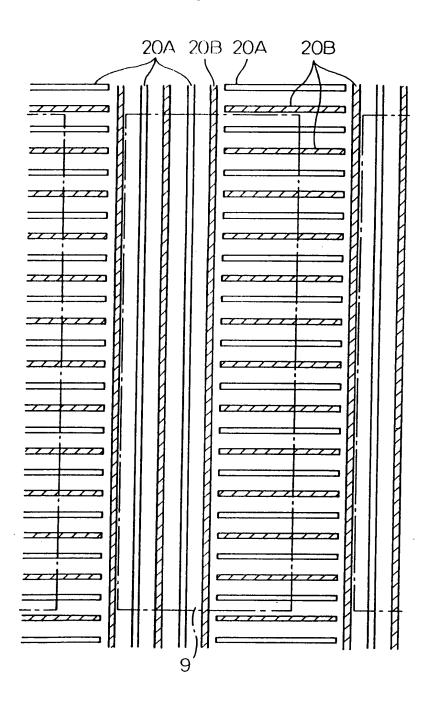




Fig. 36

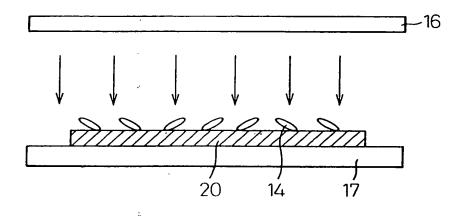


Fig.37A

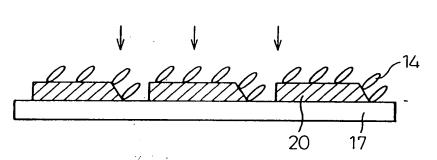


Fig.37B

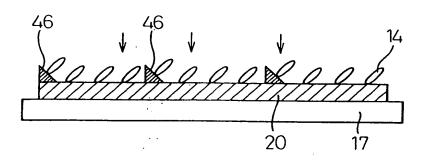




Fig.38A

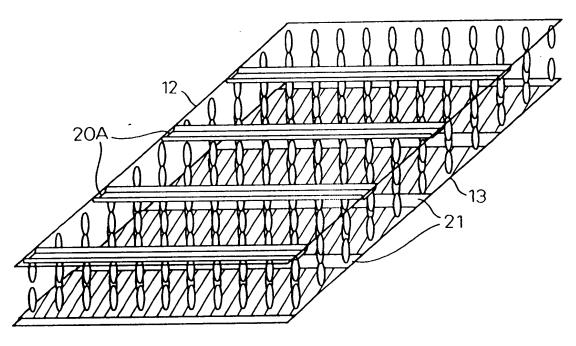


Fig.38B

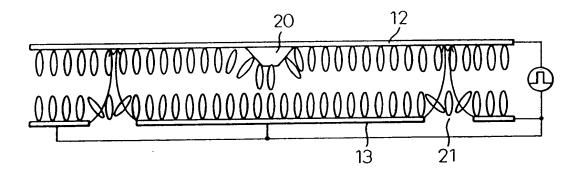




Fig.39

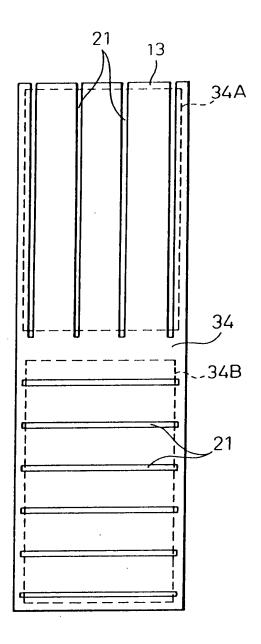




Fig.40

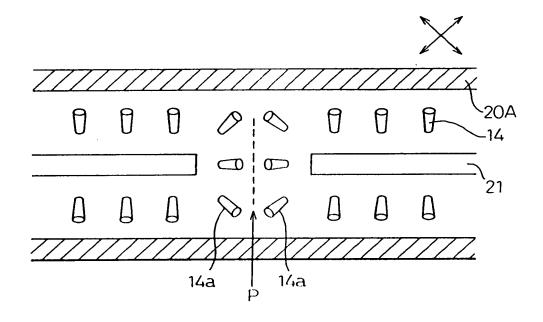


Fig.41

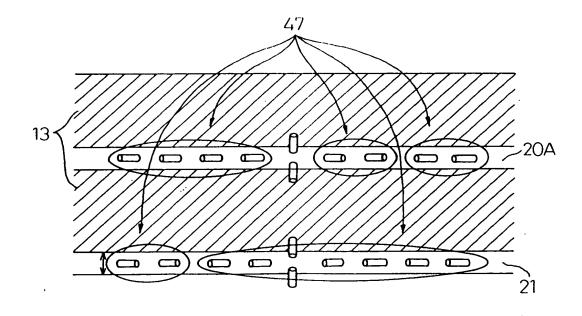




Fig.42

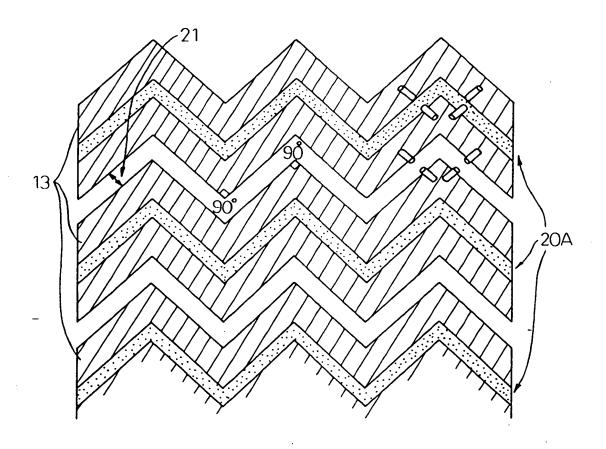
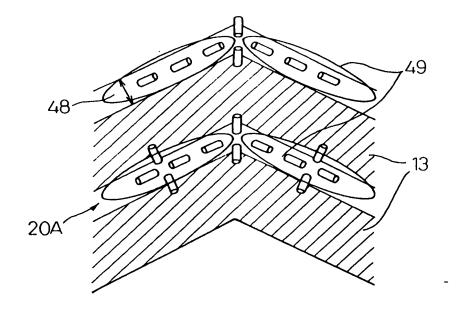




Fig.43



⁴²/₂₄₆ Fig.44

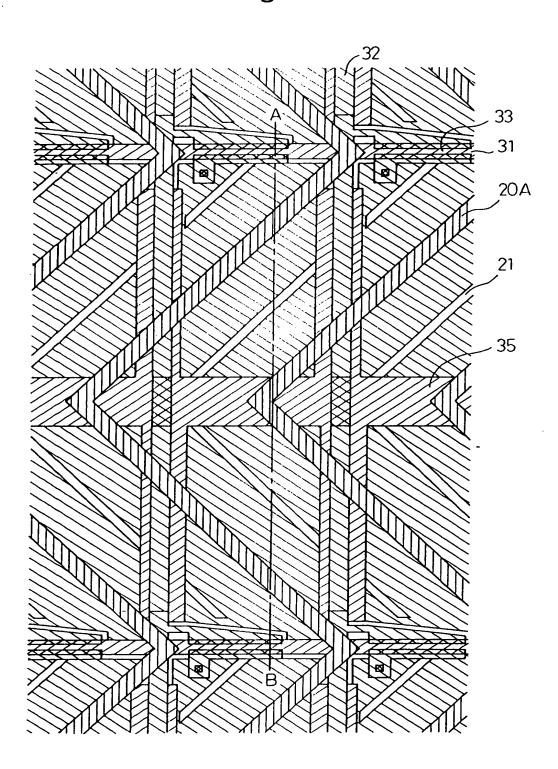
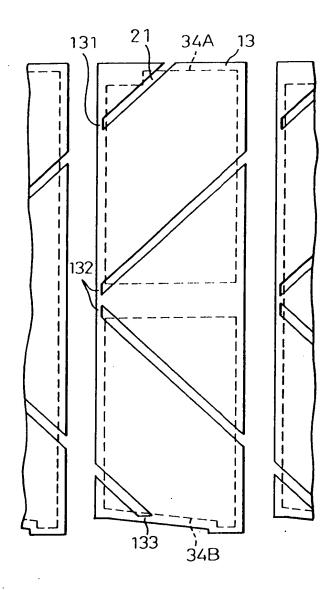




Fig.45



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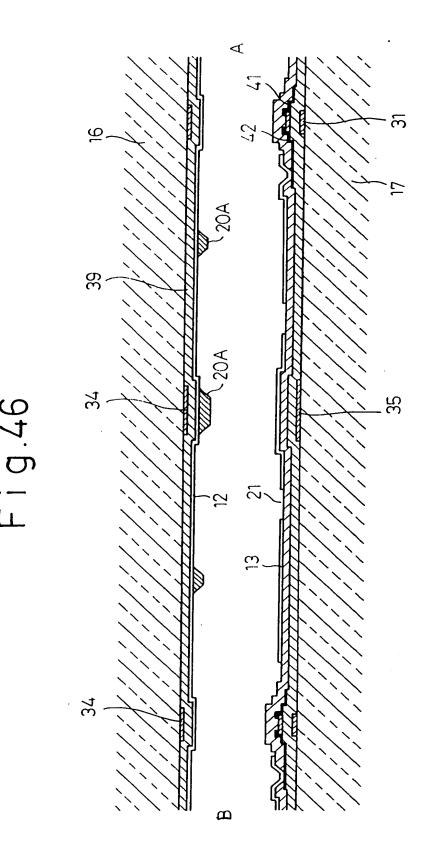




Fig.47

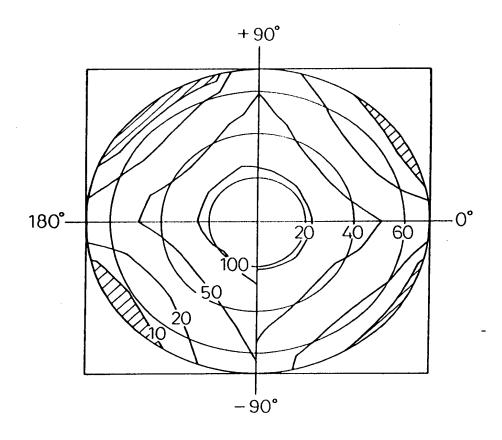




Fig.48A

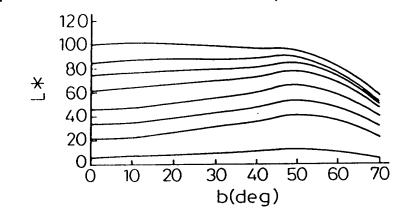
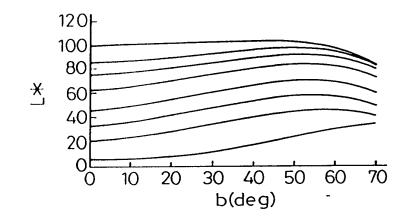


Fig.48B



-45°

- 90°

Fig.48C

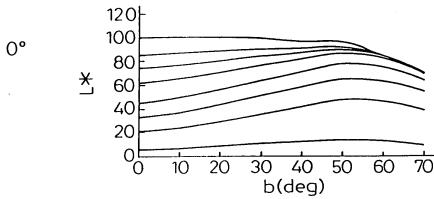




Fig.49A

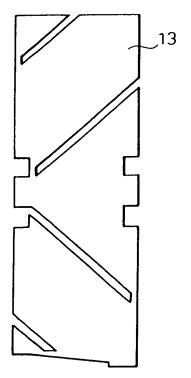
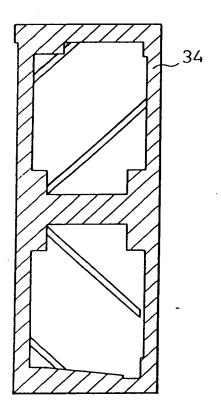


Fig.49B





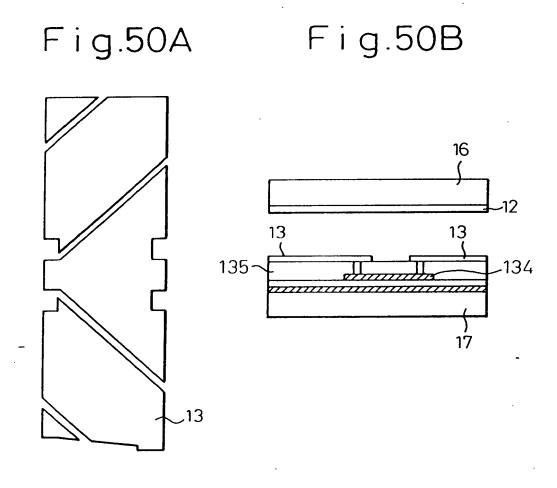




Fig.51

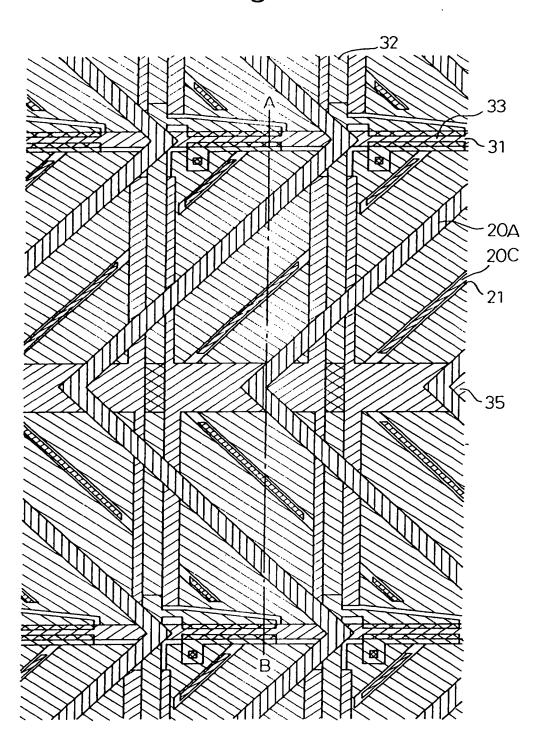
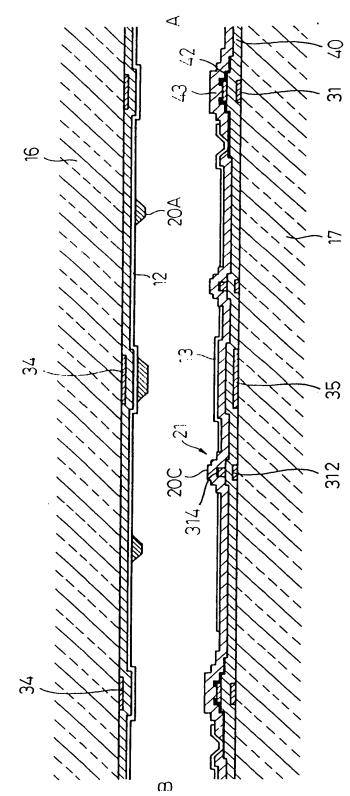


Fig.52



50/₂₄₆



Fig.53A

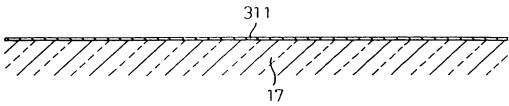


Fig. 53B

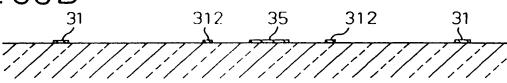


Fig.53C



Fig.53D

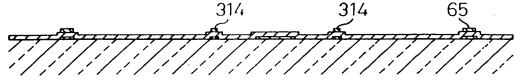


Fig.53E

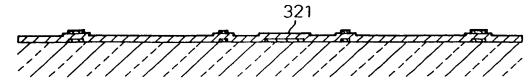




Fig.53F

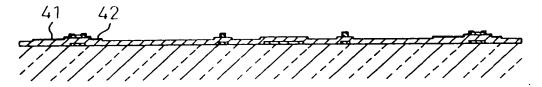


Fig.53G

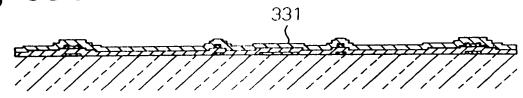


Fig. 53H

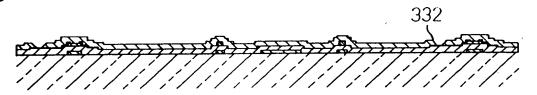


Fig. 53I

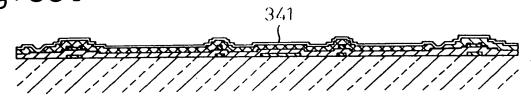


Fig. 53J

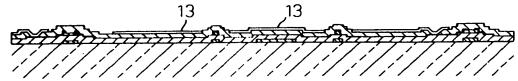
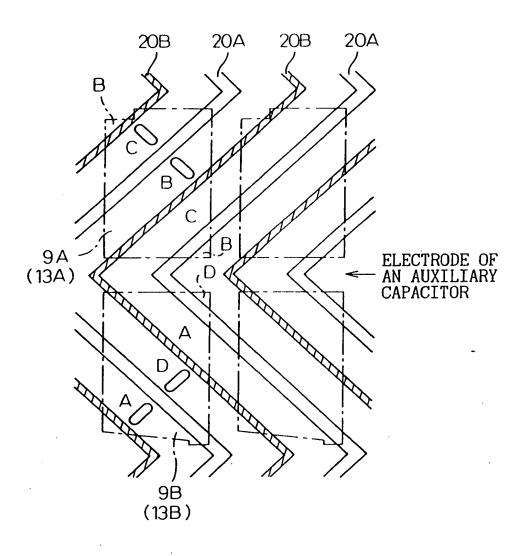




Fig.54



⁵⁴/₂₄₆ Fig.55

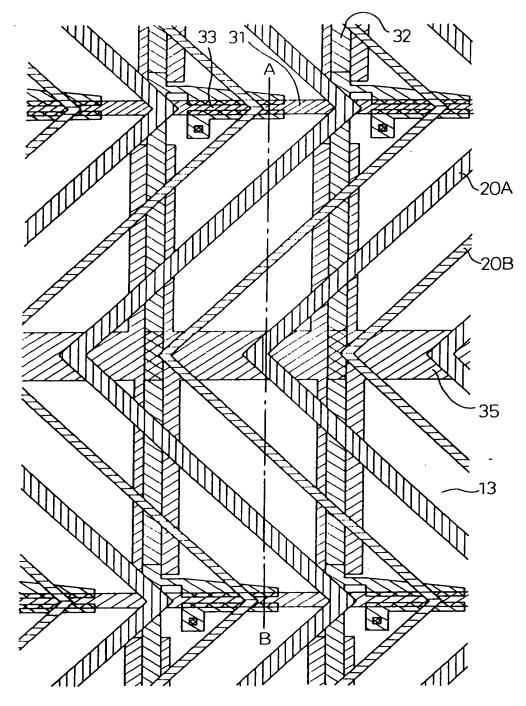




Fig.56

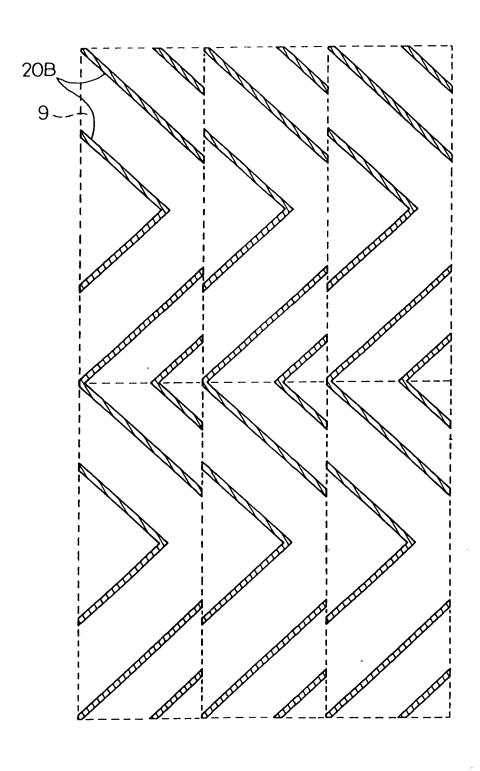




Fig.57A

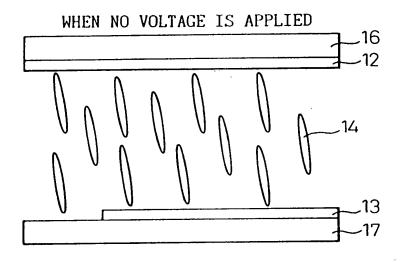


Fig.57B

WHEN A VOLTAGE IS APPLIED

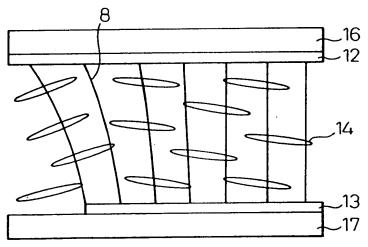




Fig.58

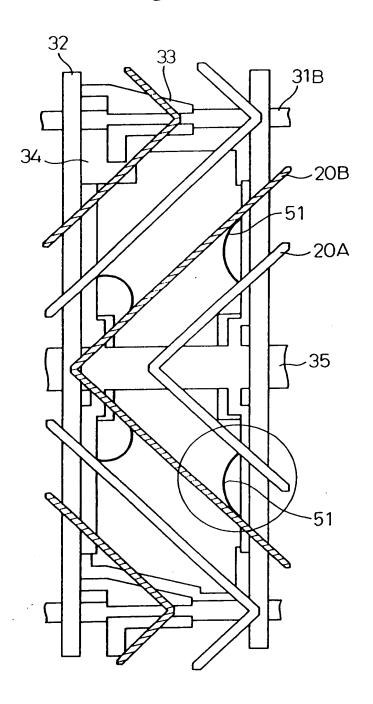




Fig.59

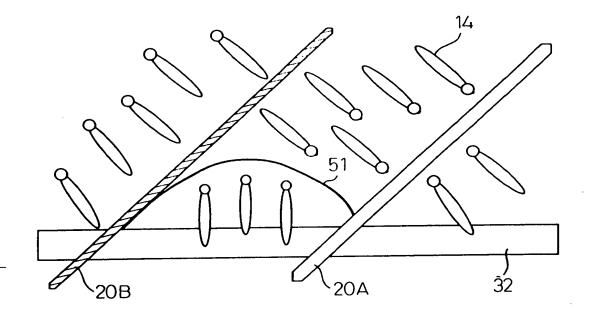




Fig. 60

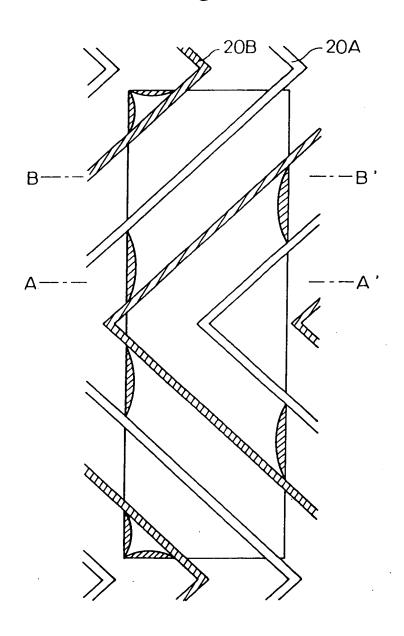




Fig.61A

A - A,

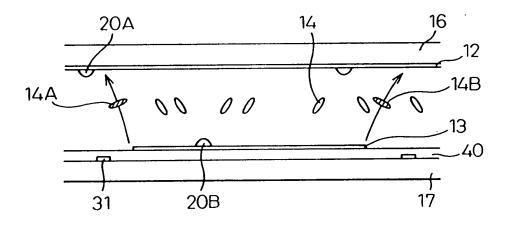


Fig.61B

B-B'

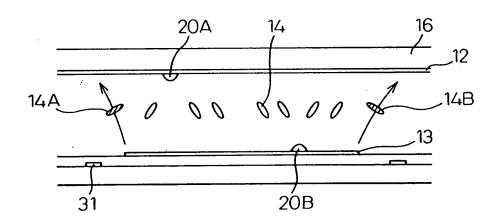




Fig.62A

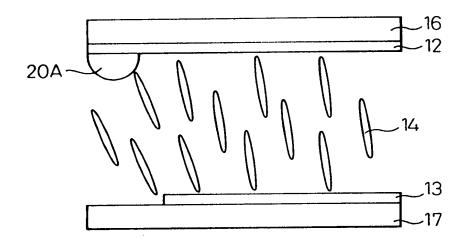


Fig.62B

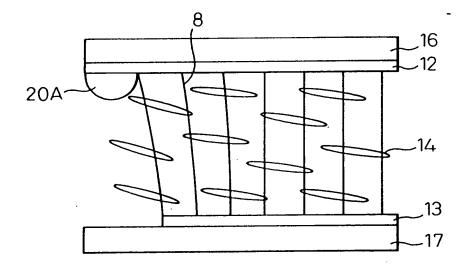




Fig. 63

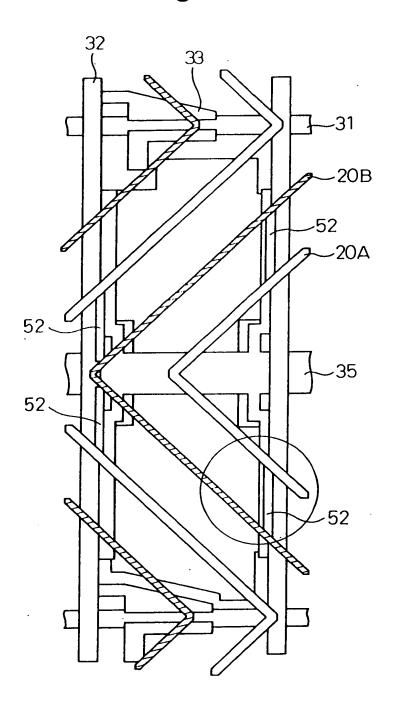




Fig.64

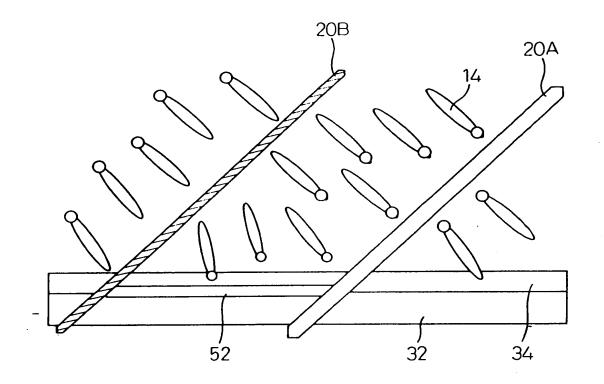




Fig.65A

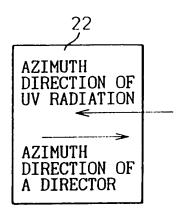


Fig.65B

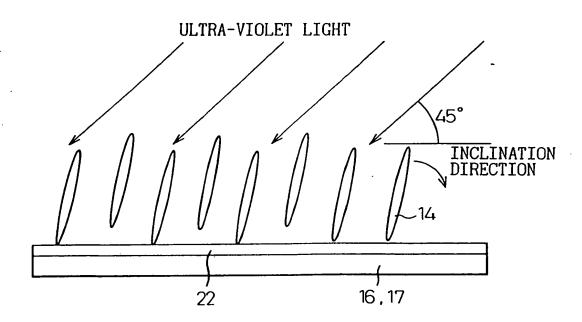
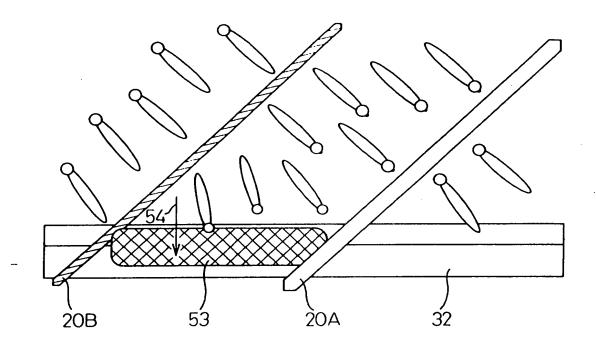
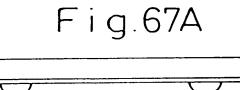




Fig.66







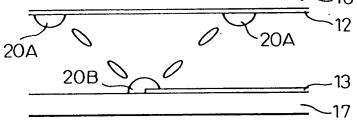


Fig.67B

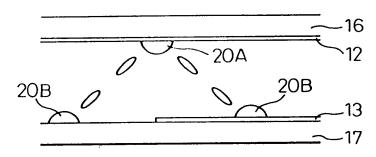


Fig.67C

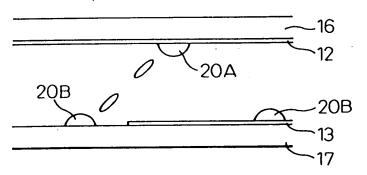




Fig.68

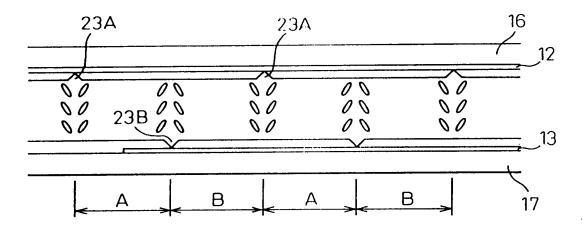




Fig.69A

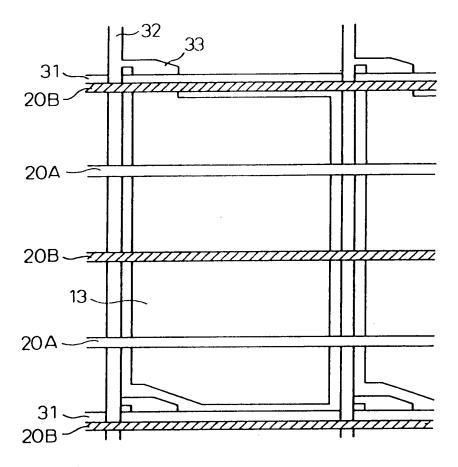
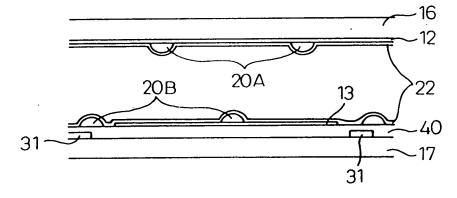
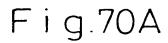


Fig.69B







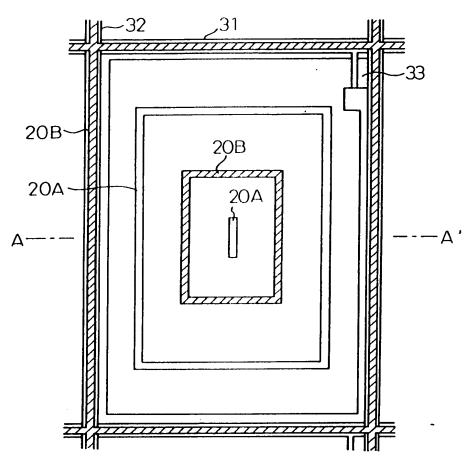


Fig.70B

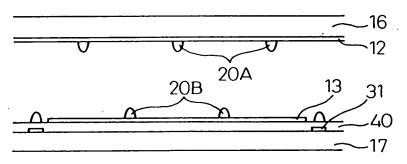




Fig.71

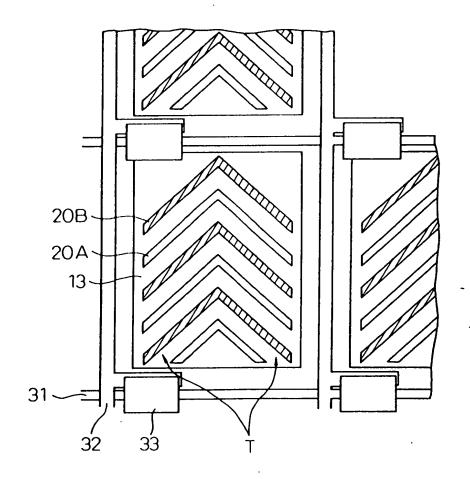




Fig.72

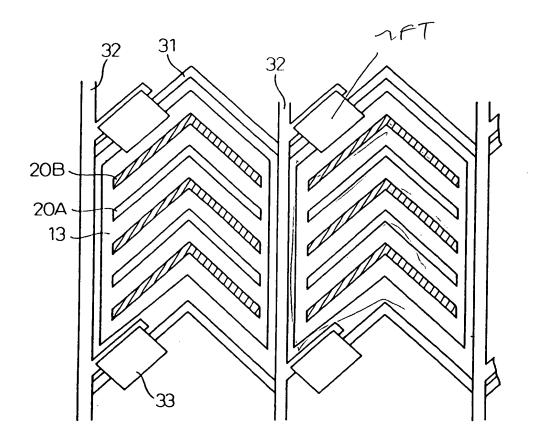




Fig.73

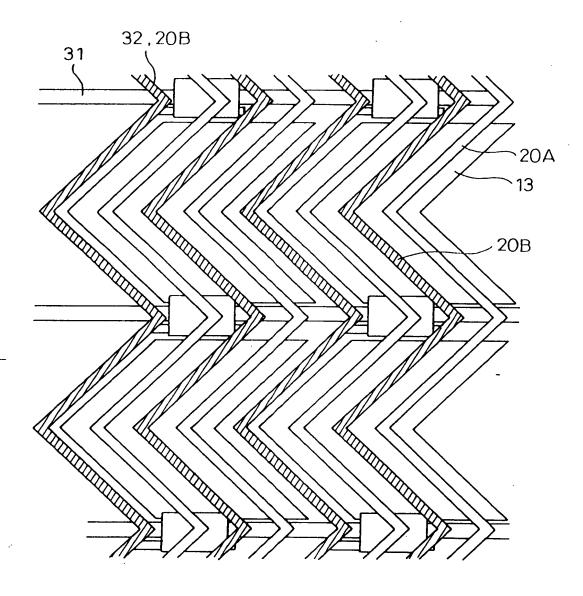




Fig.74

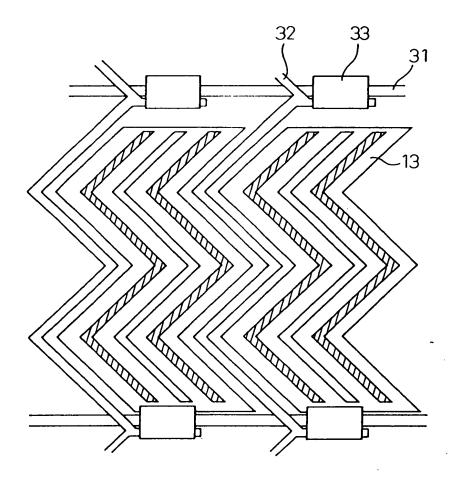




Fig.75

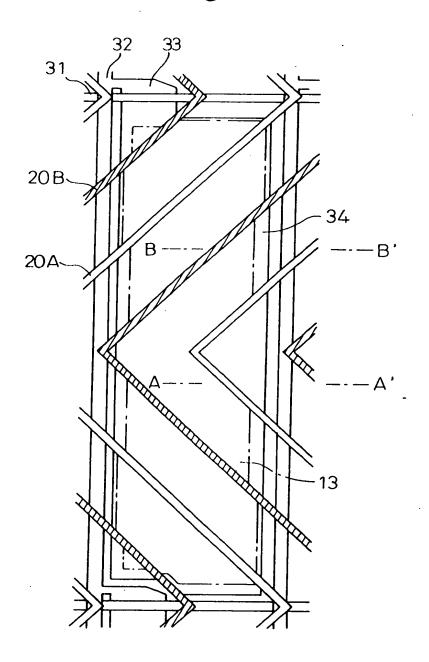




Fig.76A

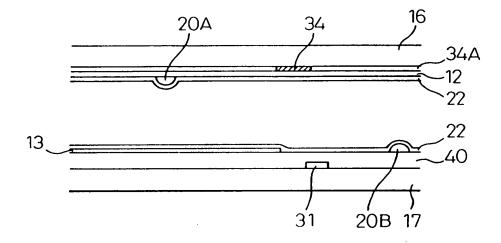


Fig.76B

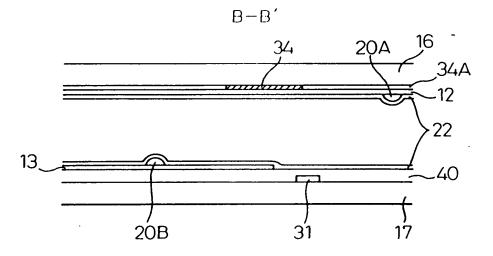




Fig.77A

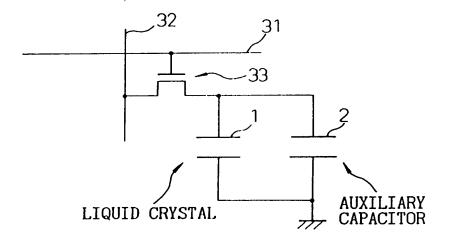


Fig.77B

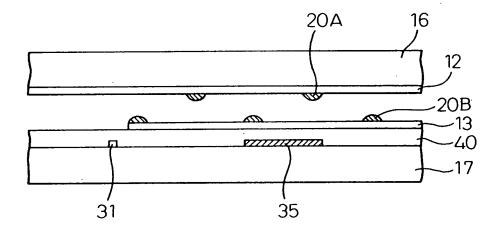




Fig.78A

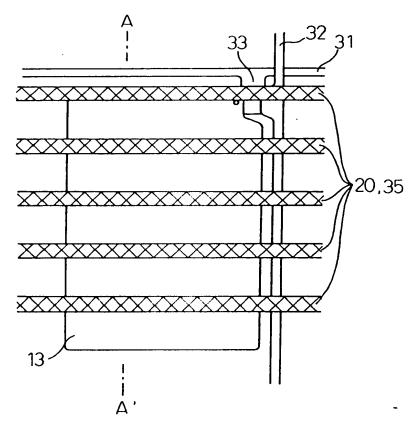


Fig.78B

20A

16

12

13

17

31

20B

35



Fig.79A

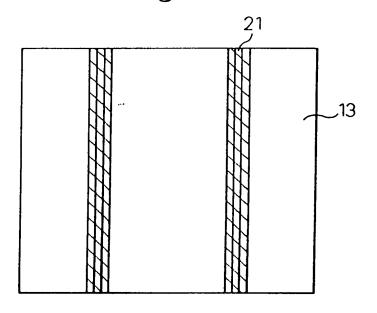


Fig.79B

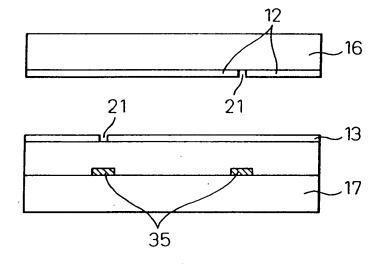




Fig.80A

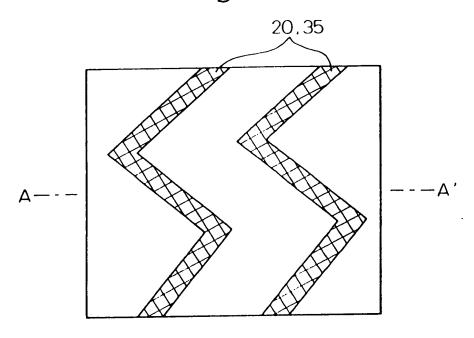


Fig.80B

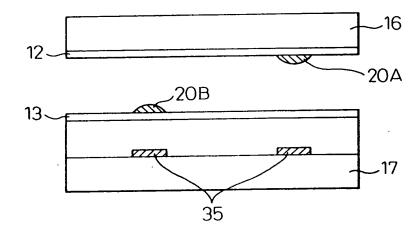




Fig.81A

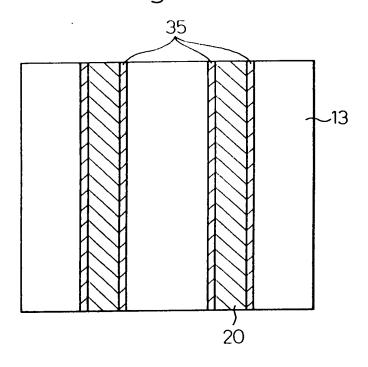


Fig.81B

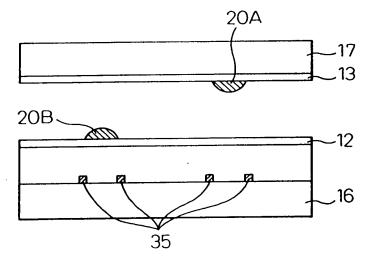
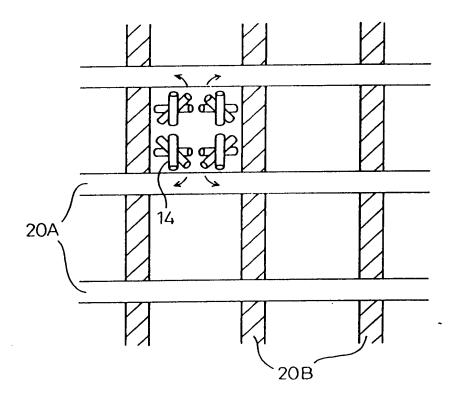




Fig.82





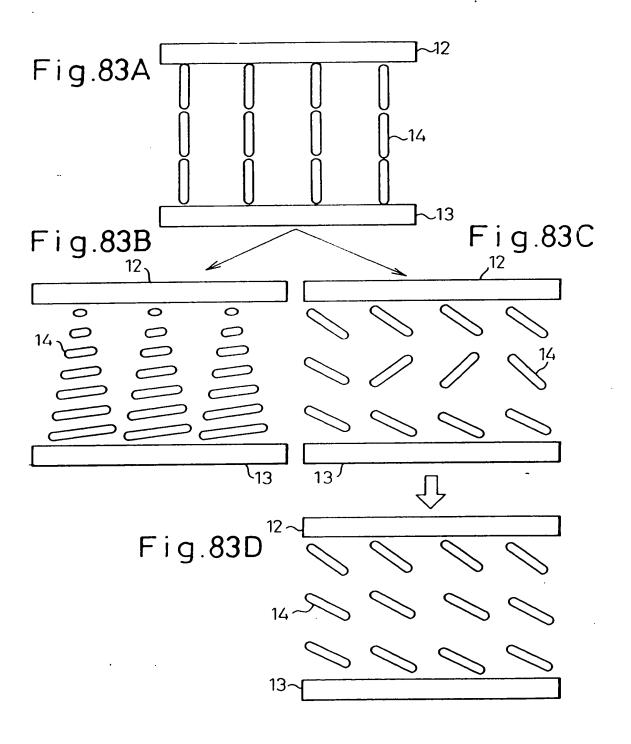
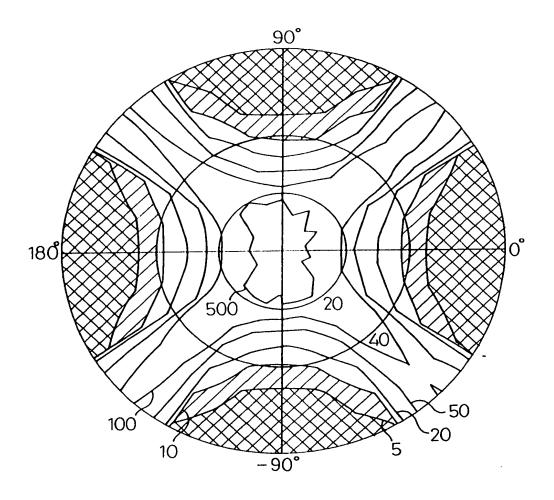
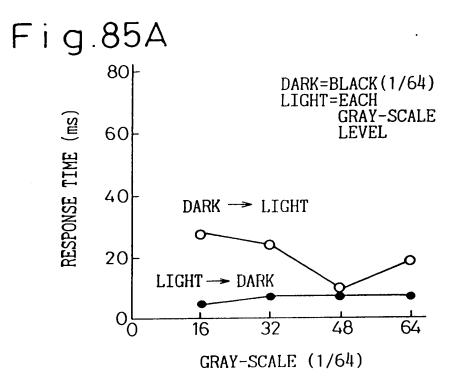


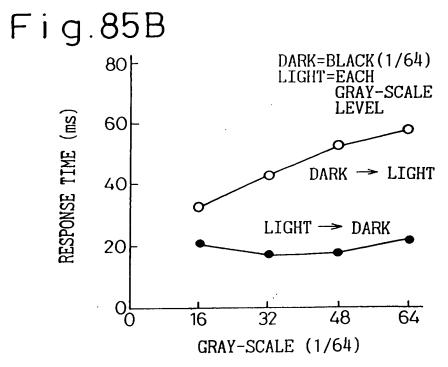


Fig.84



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85₂₄₆

Fig.85C

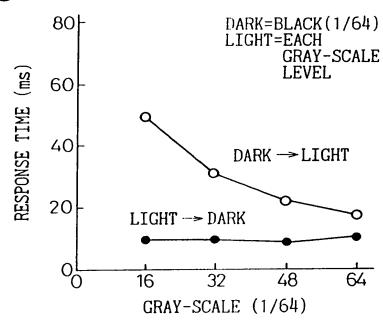
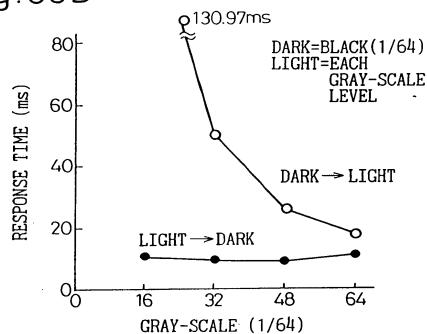


Fig.85D





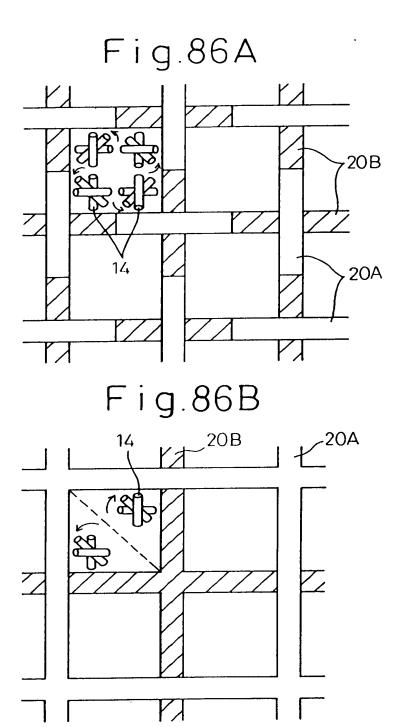






Fig.87

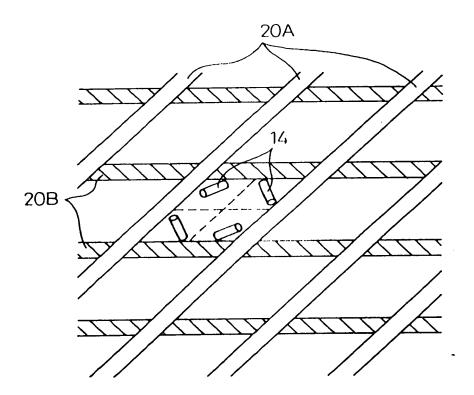




Fig. 88

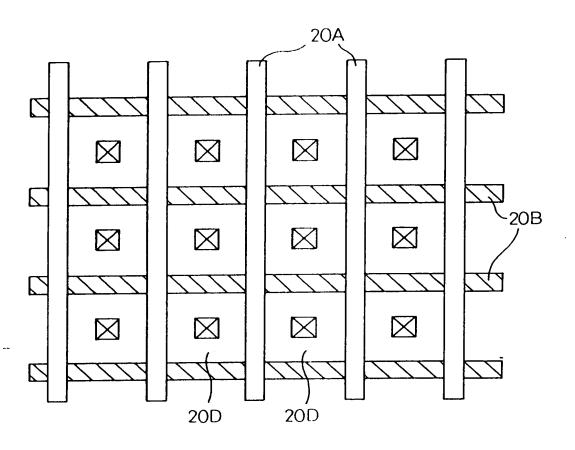




Fig.89

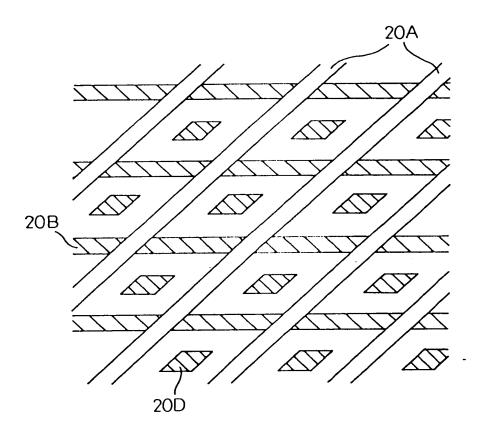




Fig.90A

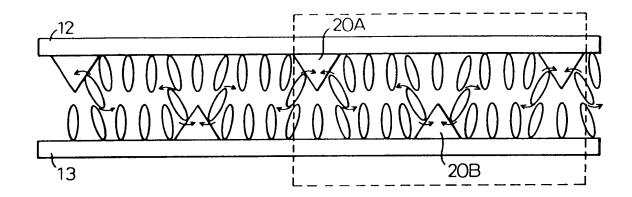


Fig.90B

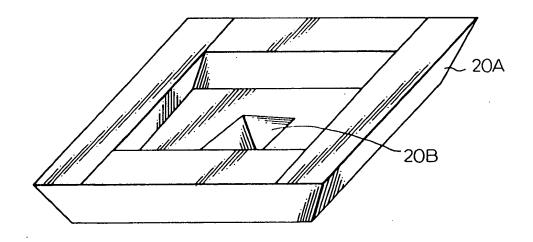




Fig.91

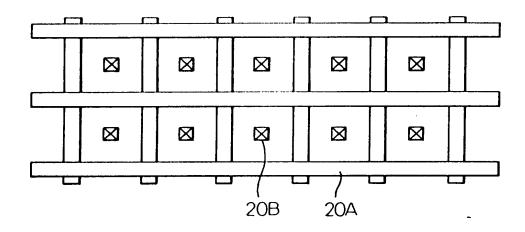




Fig.92A

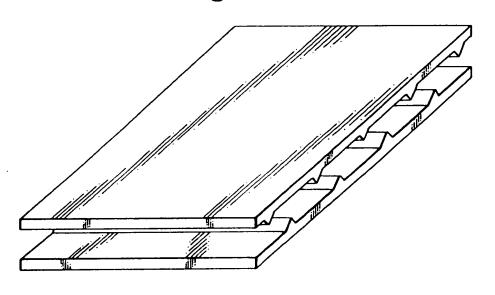
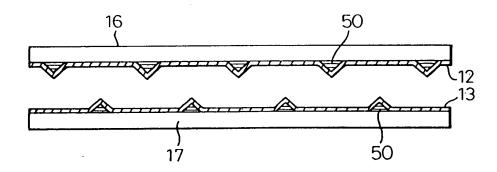


Fig.92B





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Fig.93

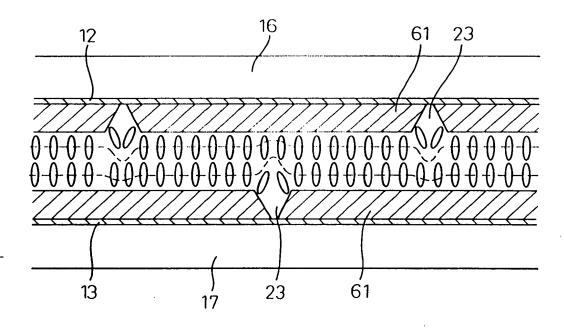




Fig.94

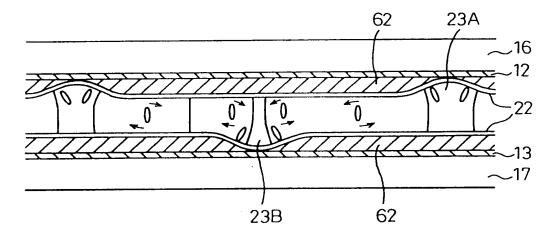


Fig.95

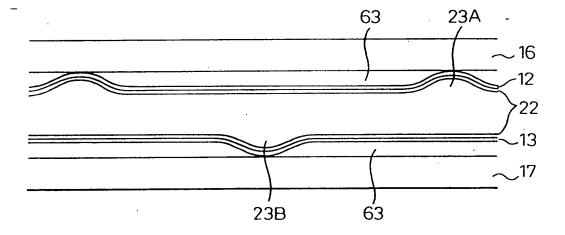




Fig.96

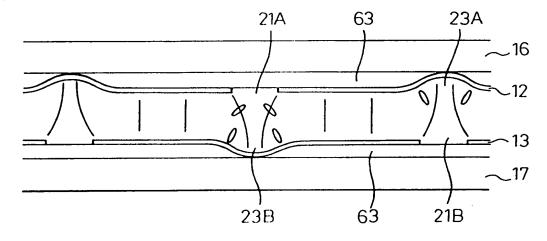


Fig.97

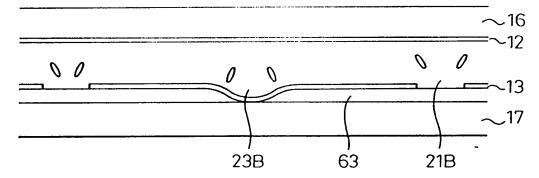


Fig.98

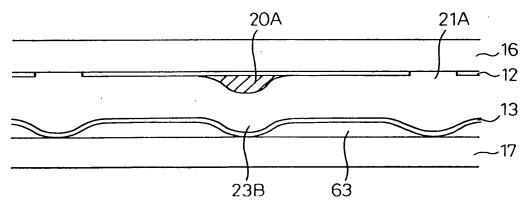




Fig.99A

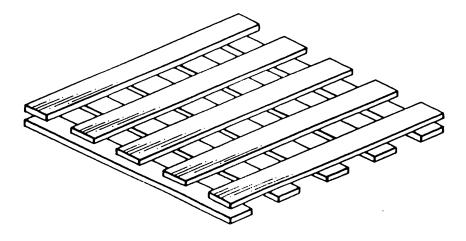
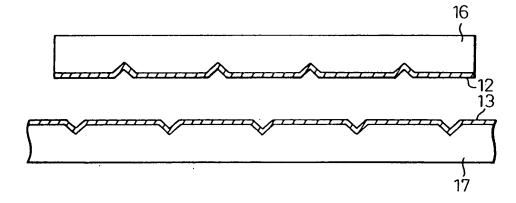


Fig.99B





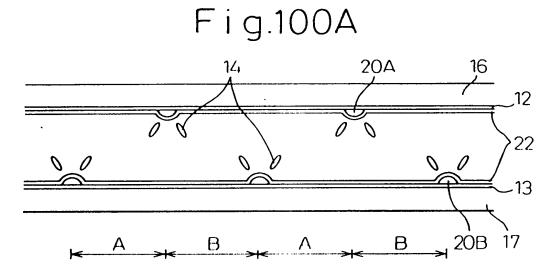


Fig.100B

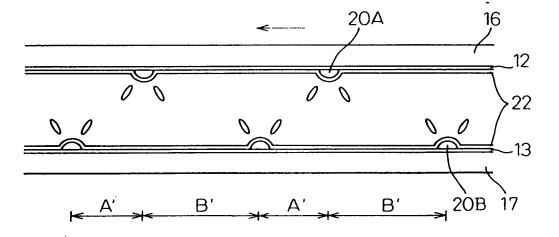




Fig.101A

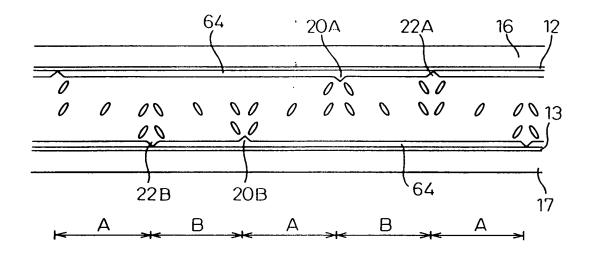


Fig.101B

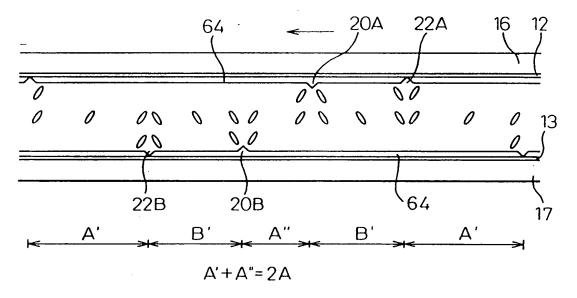
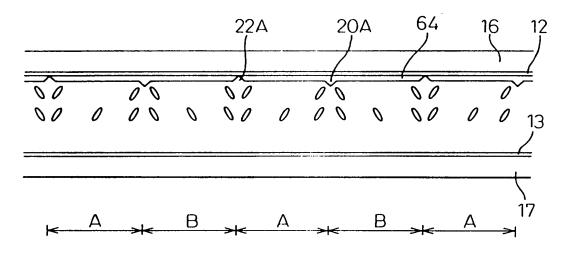




Fig.102



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Fig.103A

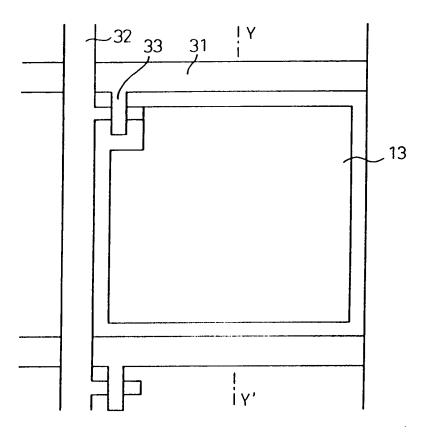


Fig. 103B

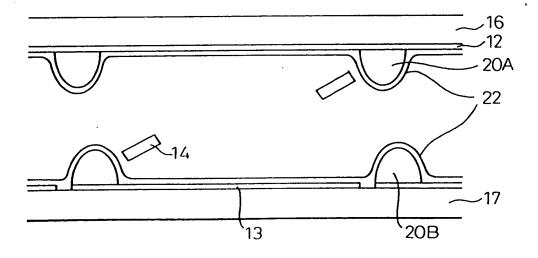
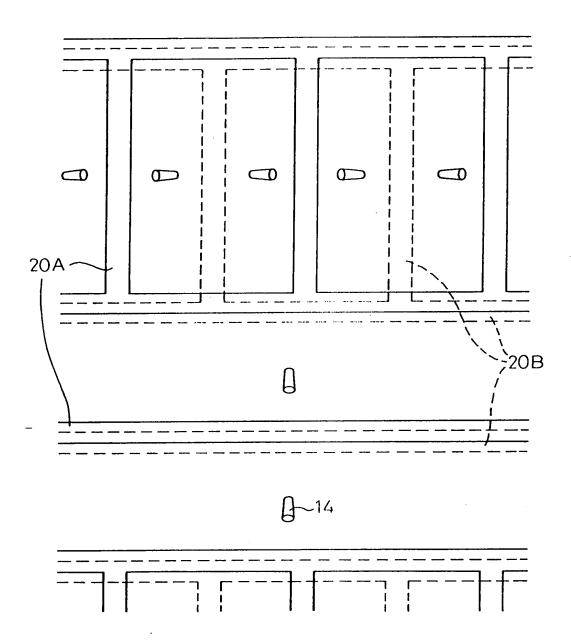




Fig.104





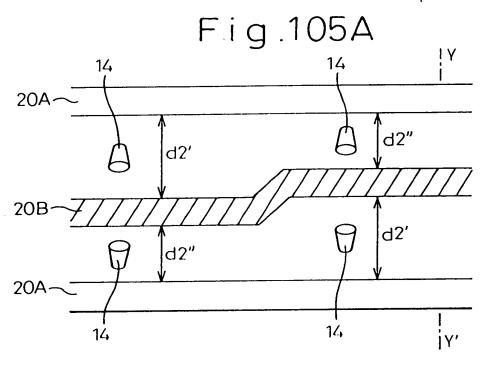


Fig.105B

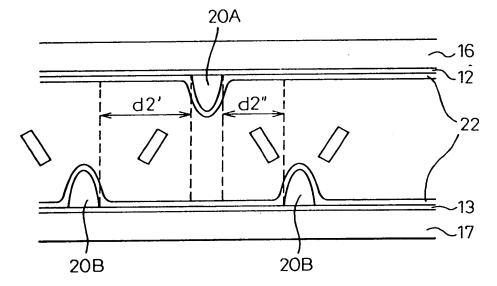




Fig.106

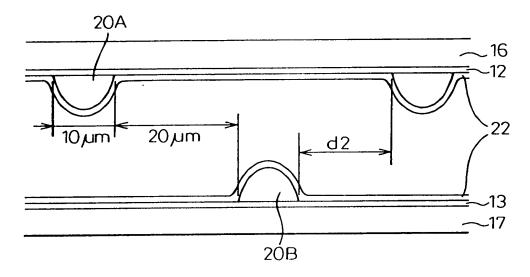
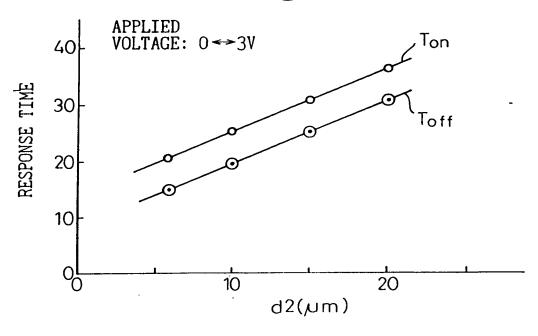


Fig.107



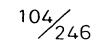


Fig.108A

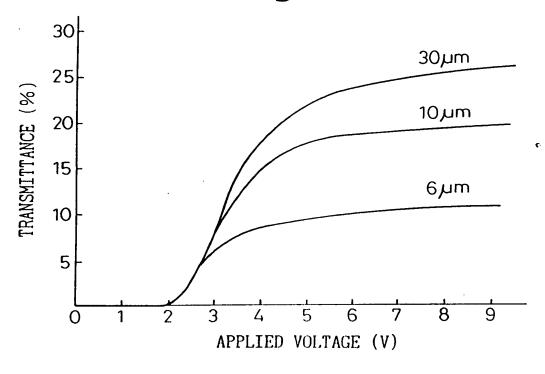


Fig.108B

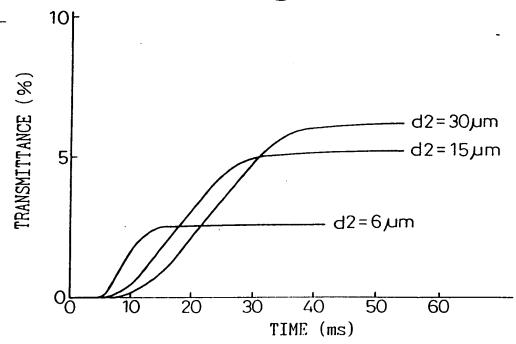




Fig.109A

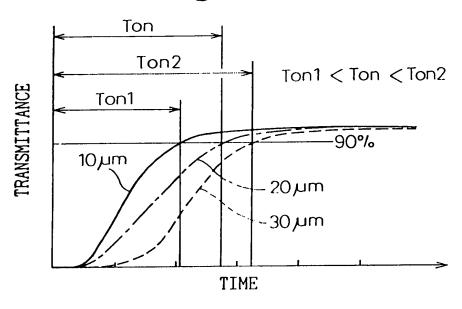


Fig.109B

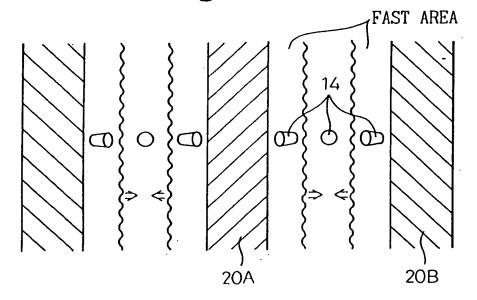




Fig.110

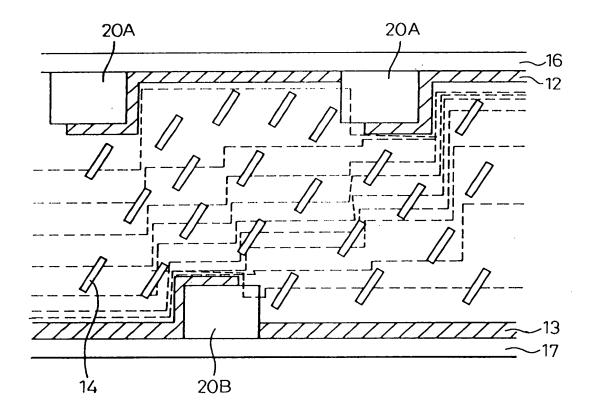




Fig. 111

CONTRAST RATIO

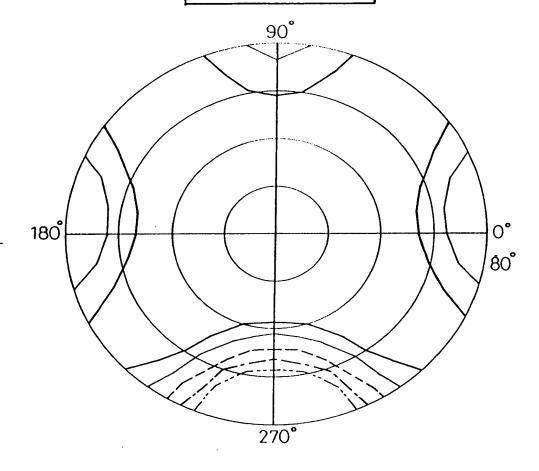




Fig.112

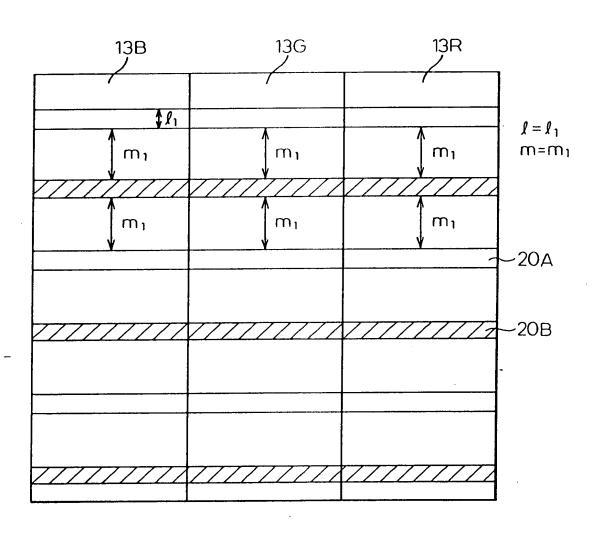




Fig.113

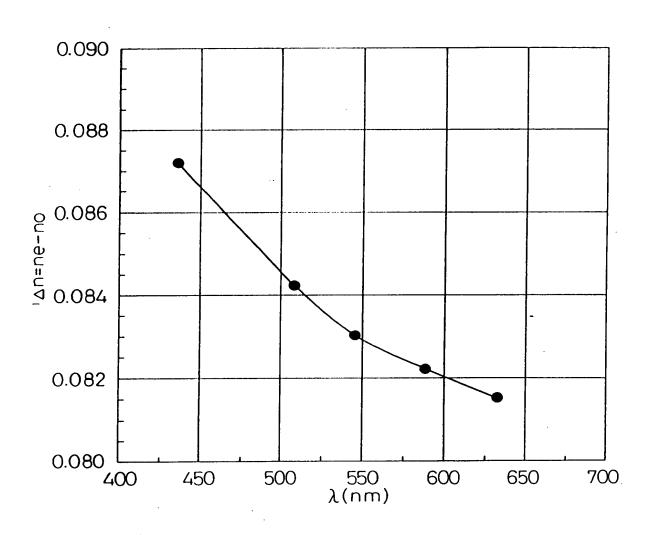




Fig.114

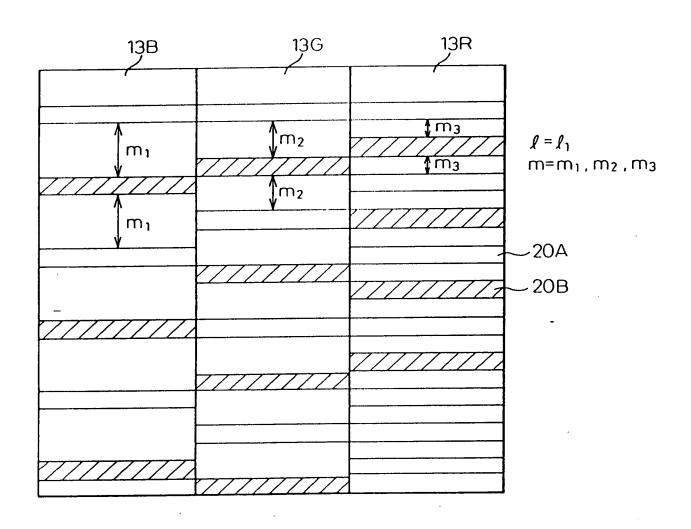




Fig.115

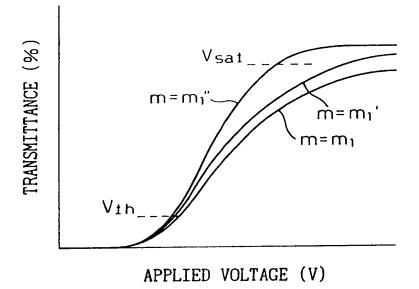




Fig.116

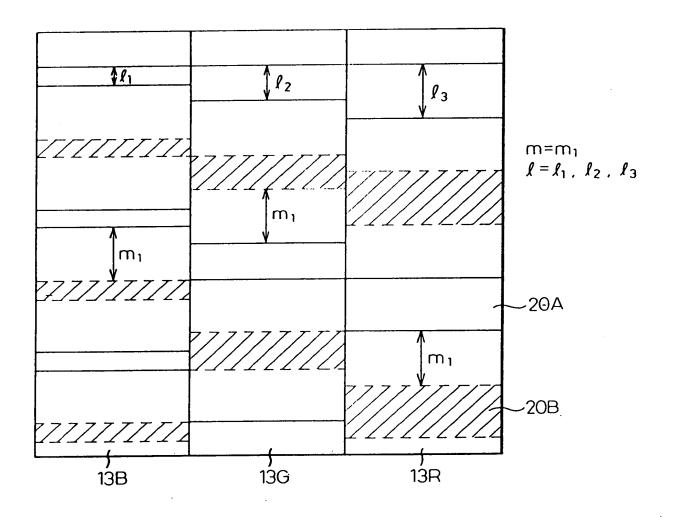




Fig.117

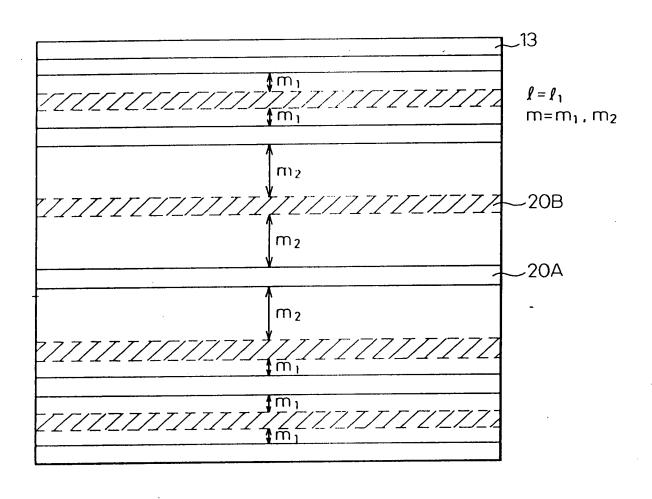
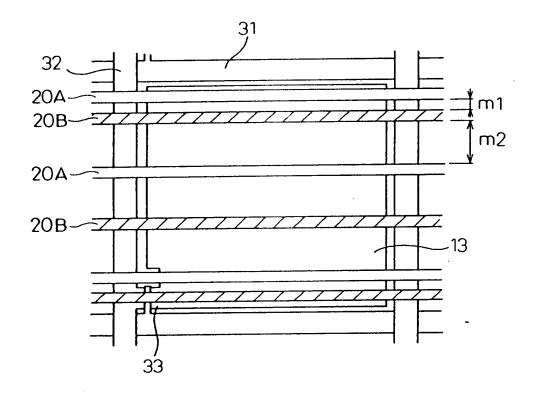




Fig.118



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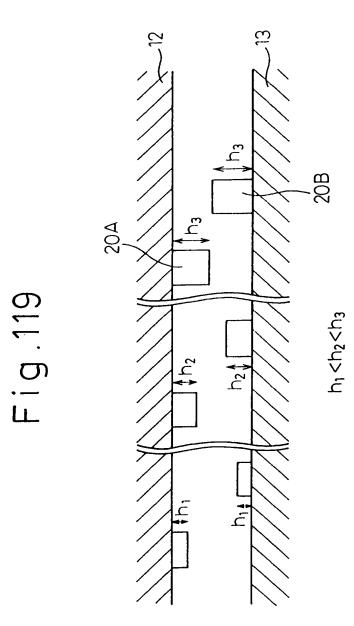
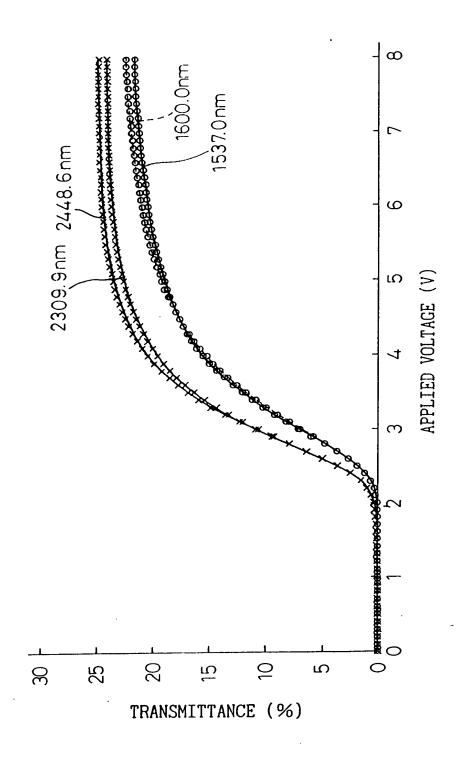


Fig.120

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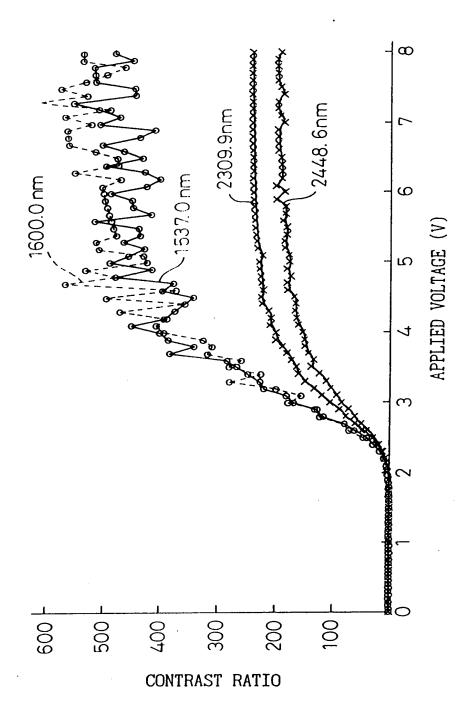
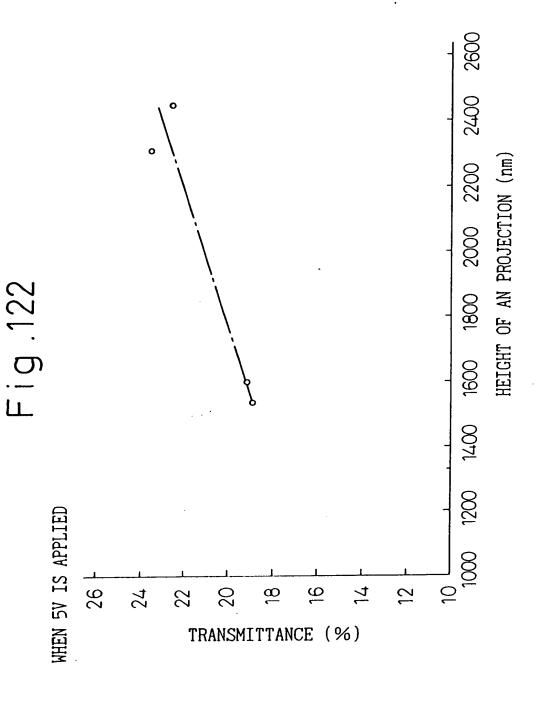
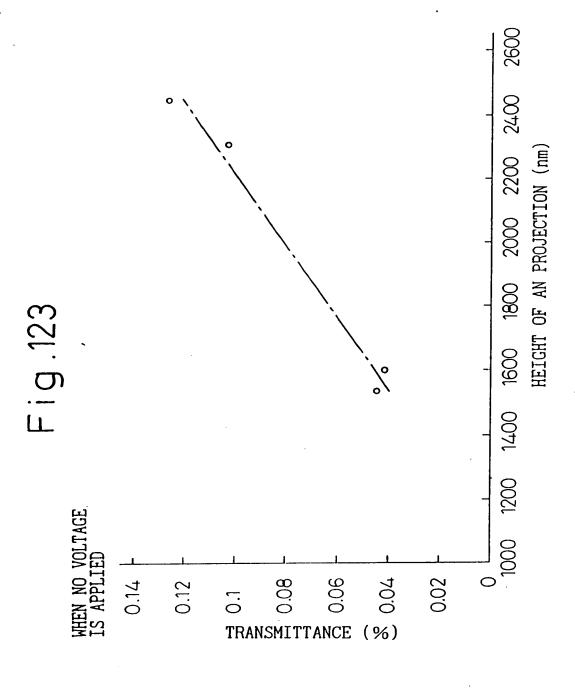


Fig.121





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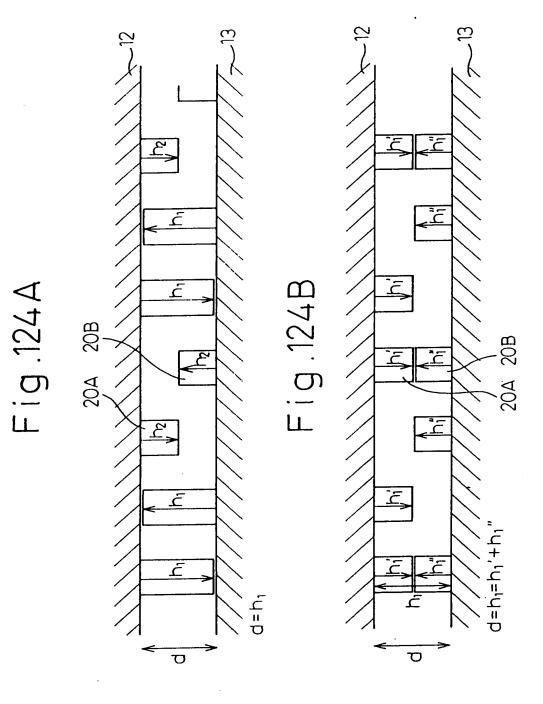


Fig.125A

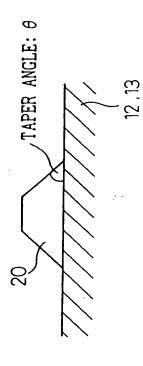
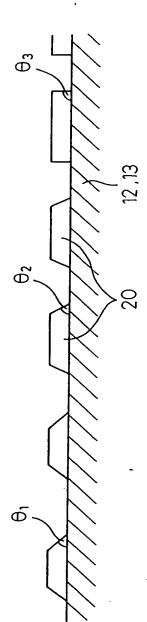


Fig.125B



 $\theta_1 < \theta_2 < \theta_3$

Fig.126

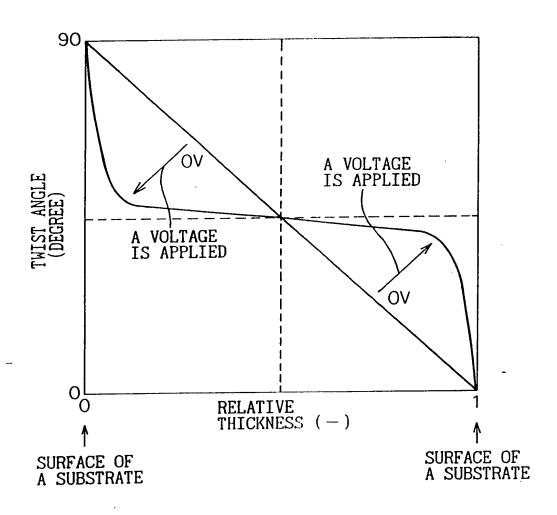




Fig. 127

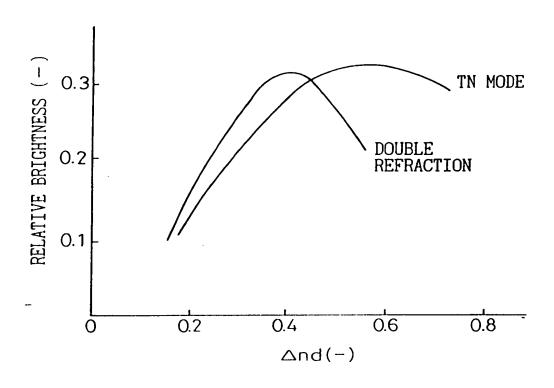


Fig .128

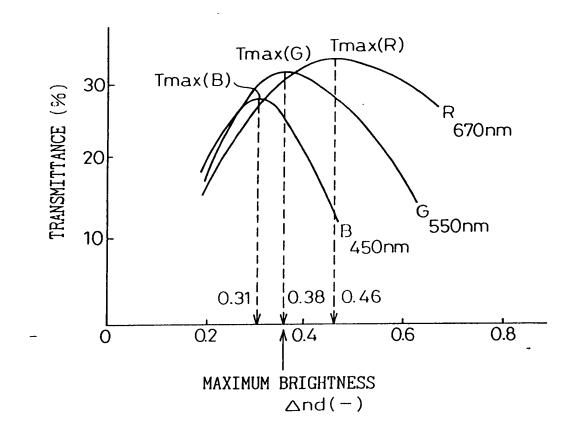


Fig.129

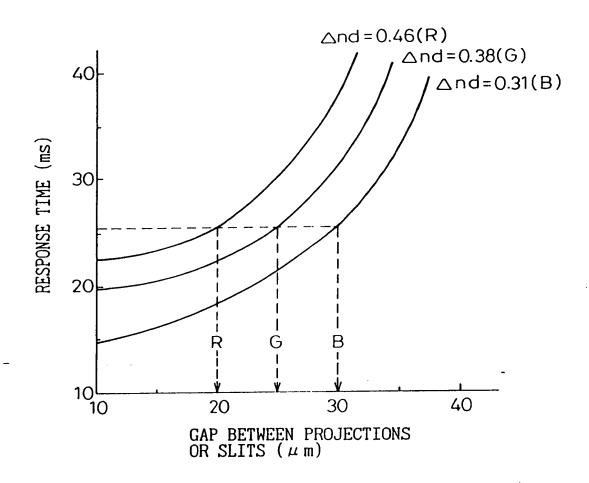
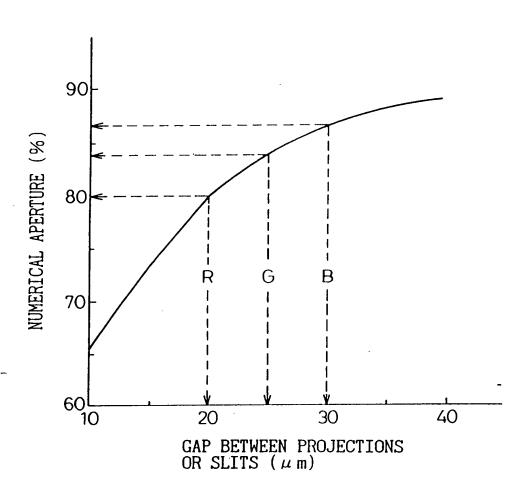
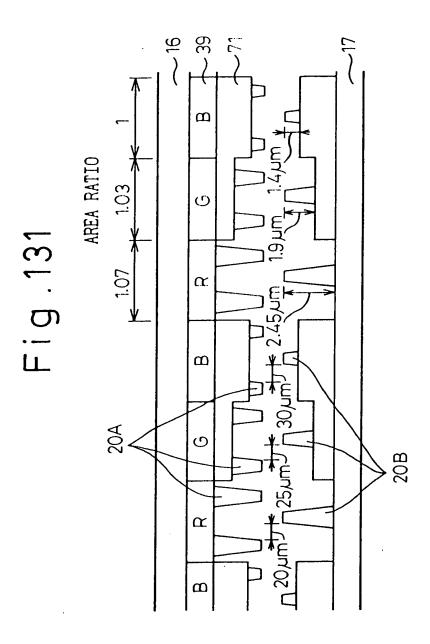


Fig.130







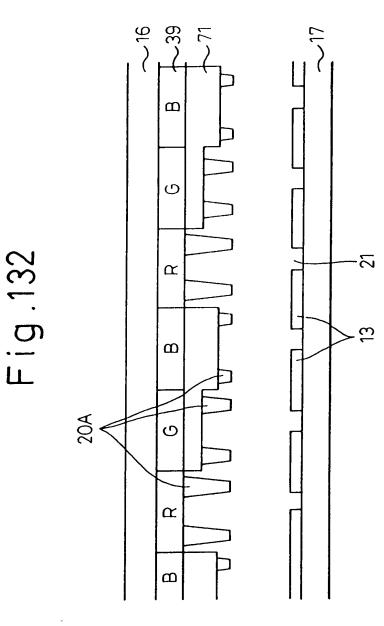




Fig.133

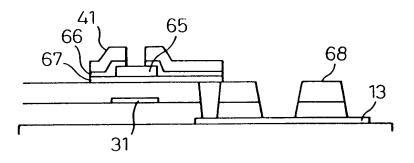
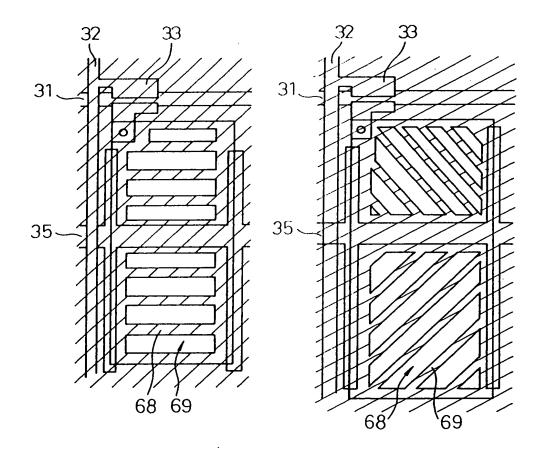


Fig.134A

Fig.134B



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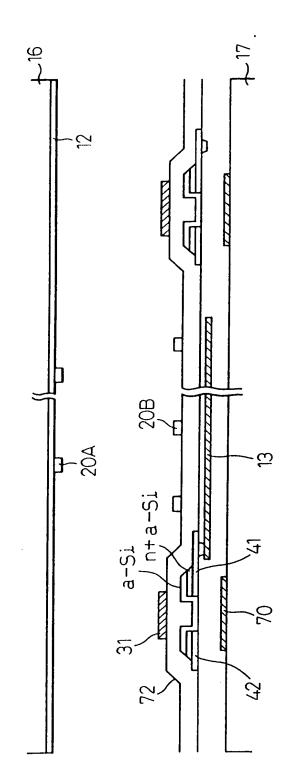
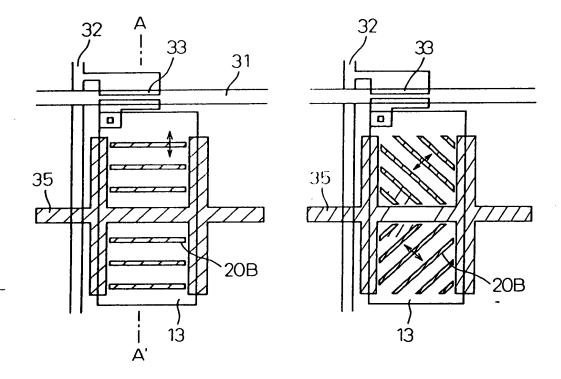


Fig.135

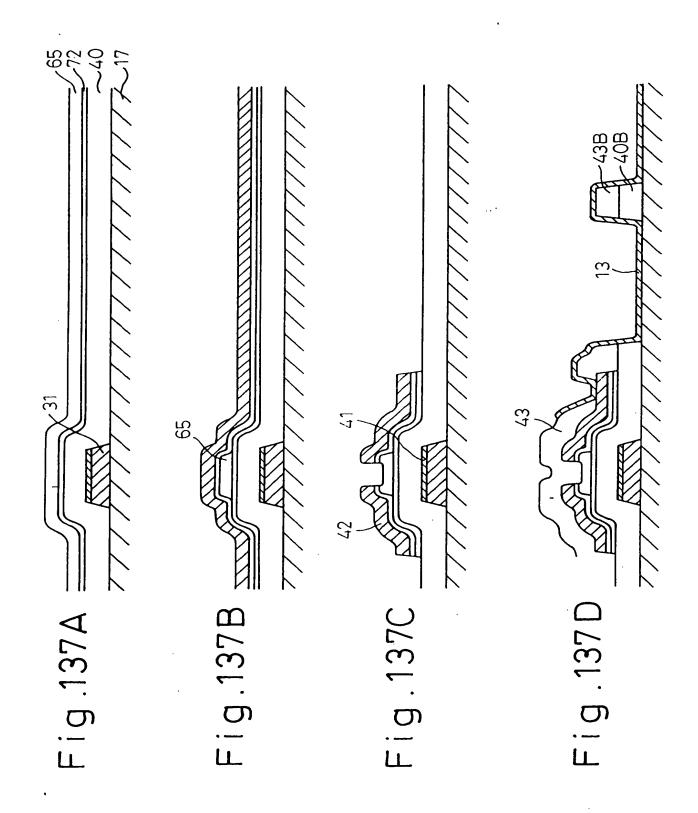


Fig.136A

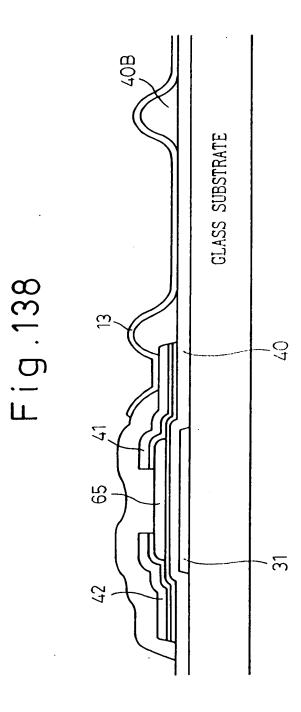
Fig.136B







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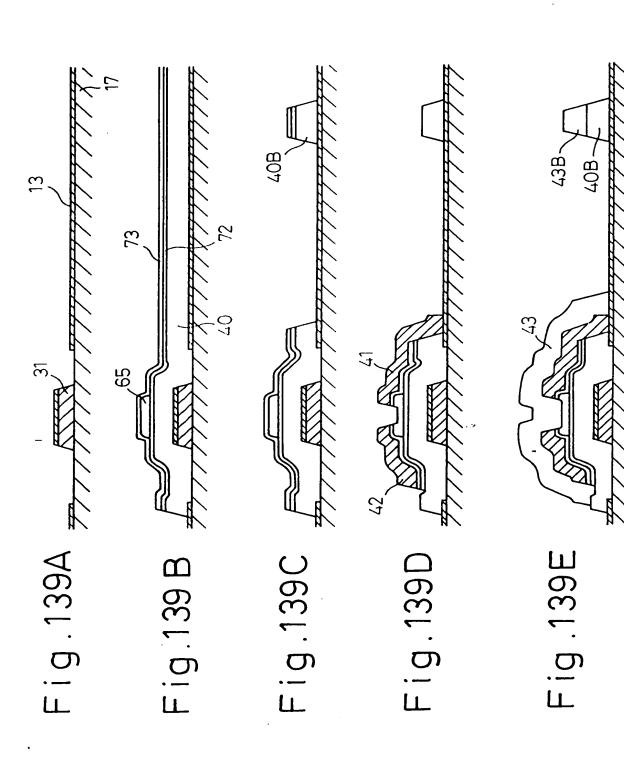




Fig.140A

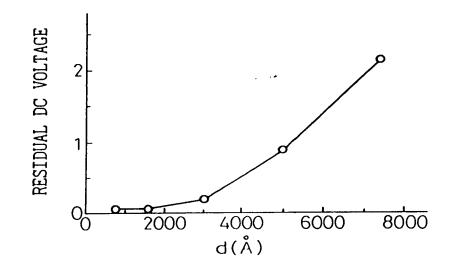


Fig.140B

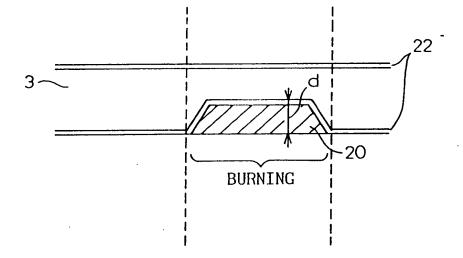




Fig.141A

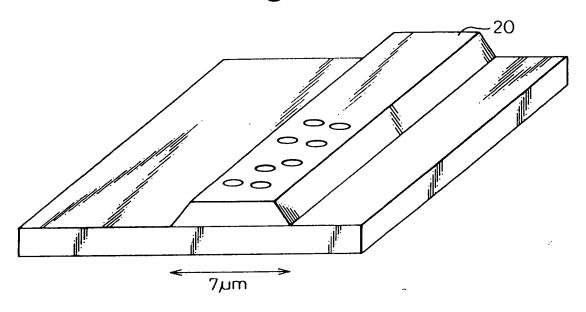
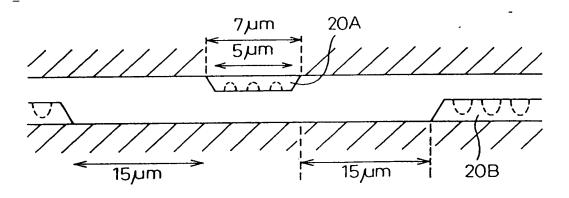


Fig.141B



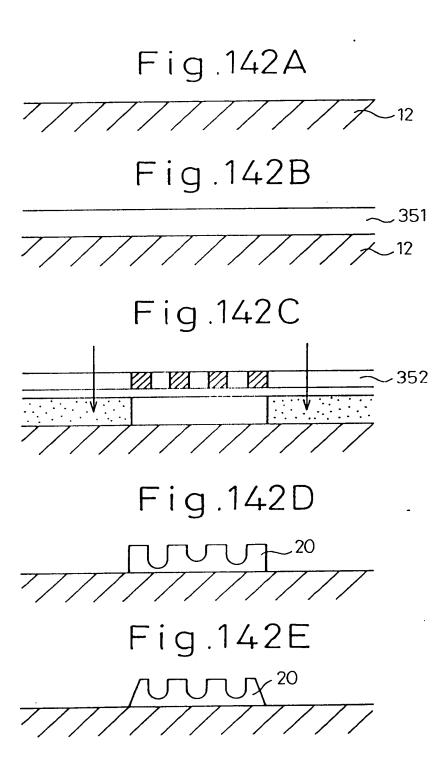
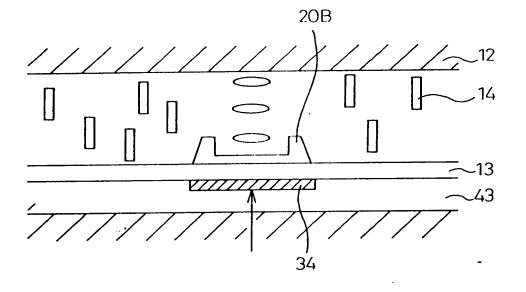
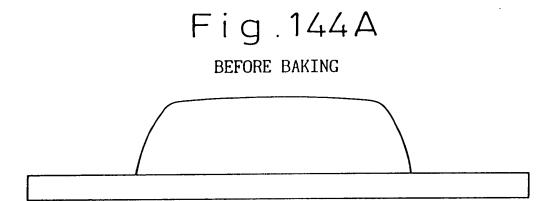




Fig.143





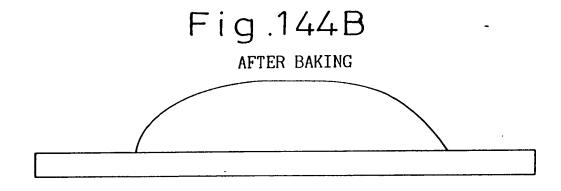




Fig.145A

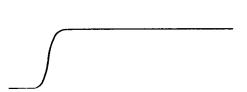
NO BAKING

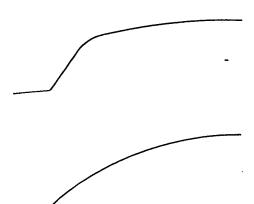
Fig.145B 120°C

Fig.145C 130℃

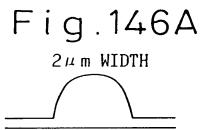
Fig.145D 140°C

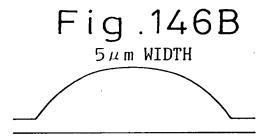
Fig.145E 150°C











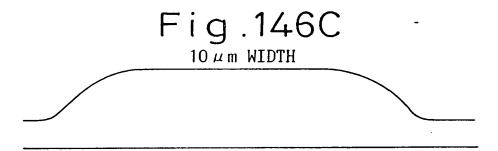




Fig.147A

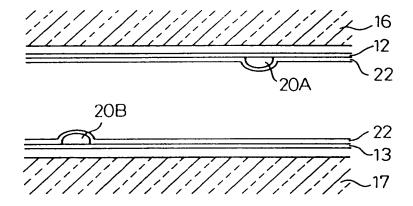


Fig.147B

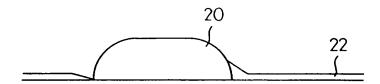




Fig.148A

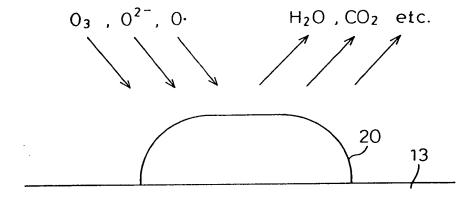


Fig.148B

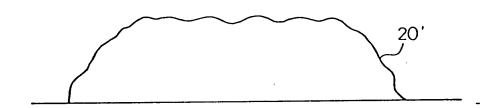


Fig.148C

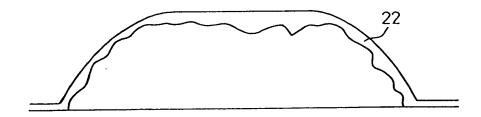




Fig.149A

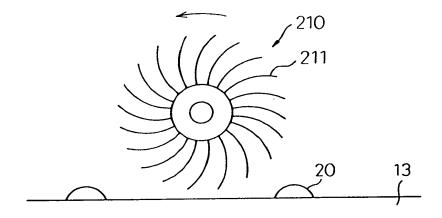


Fig.149B

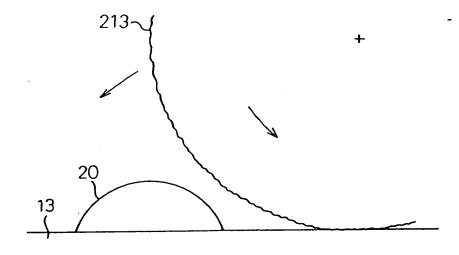
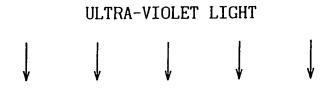




Fig.150



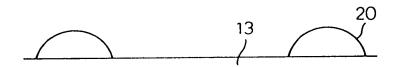




Fig.151A

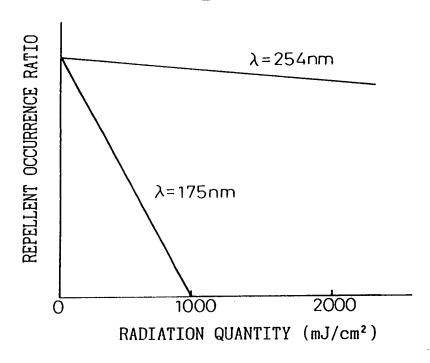


Fig.151B

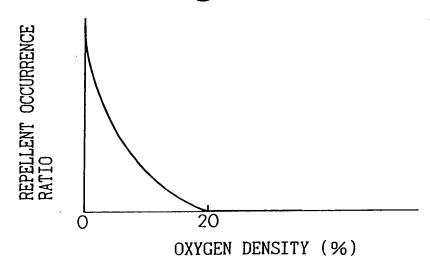




Fig.152A

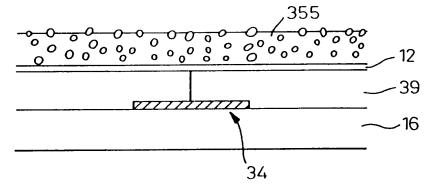


Fig.152B

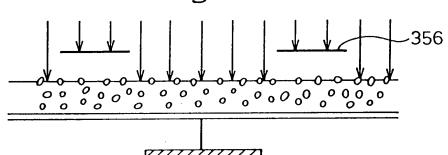


Fig.152C

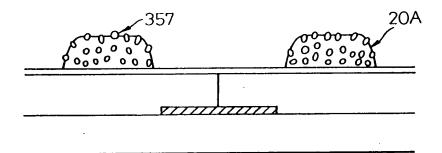




Fig.153A

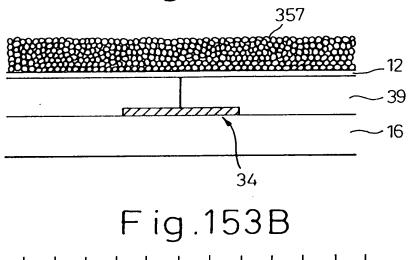


Fig.153C

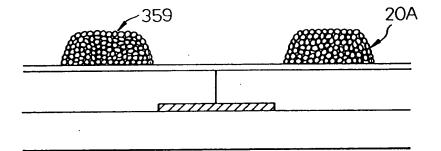




Fig.154A

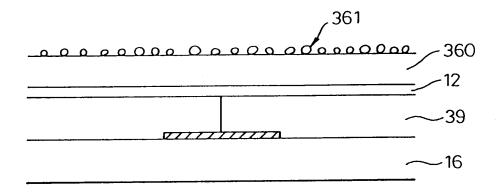
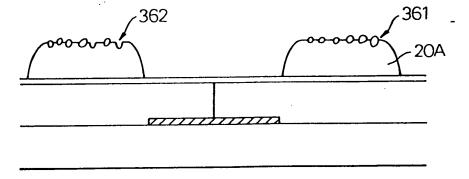


Fig.154B



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Fig.155A

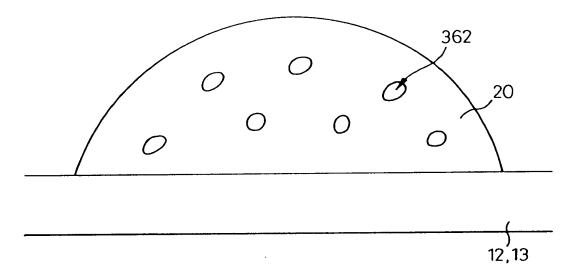
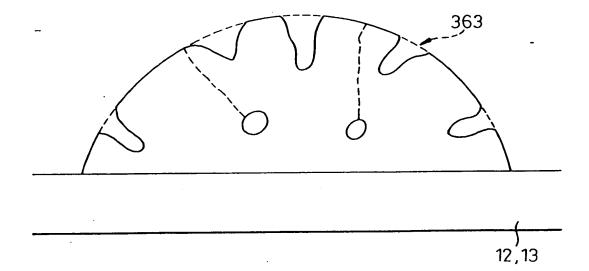


Fig.155B





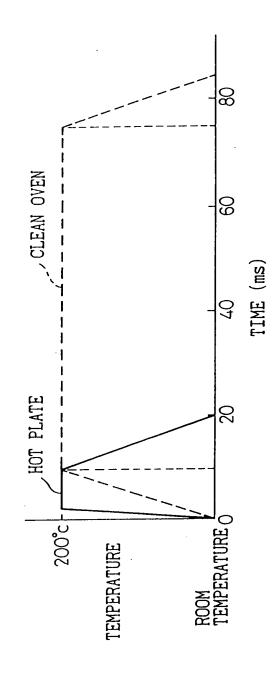


Fig.156



Fig.157A

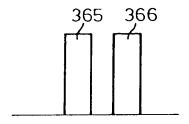


Fig.157B

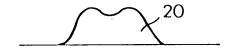
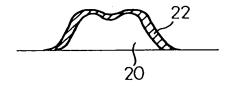


Fig.157C



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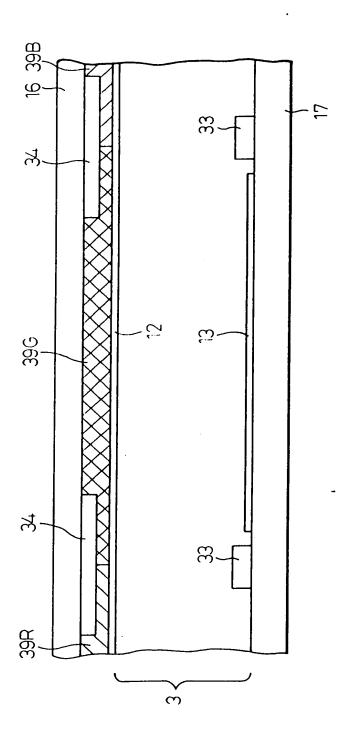


Fig.158

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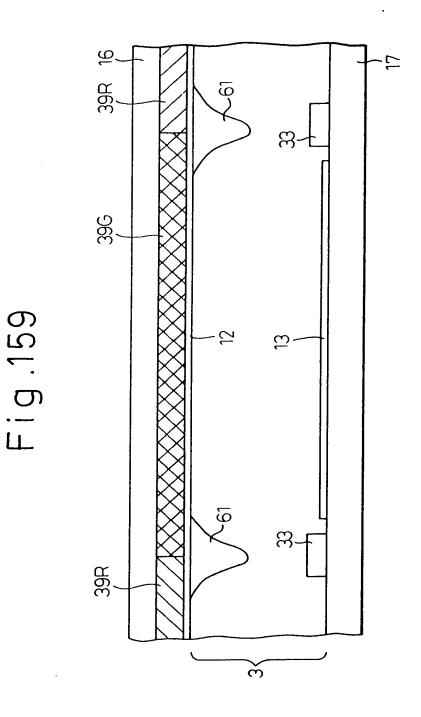
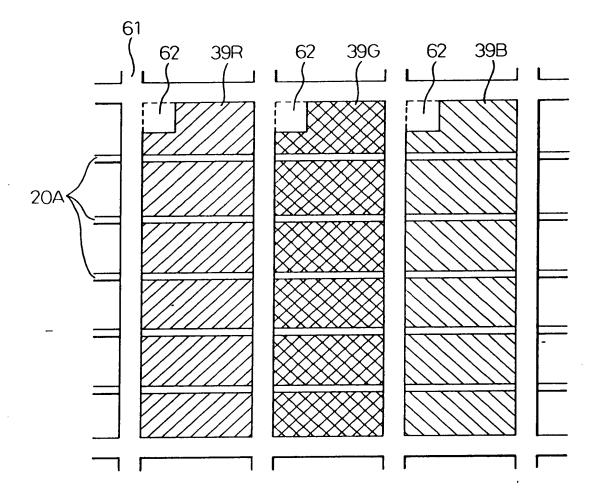
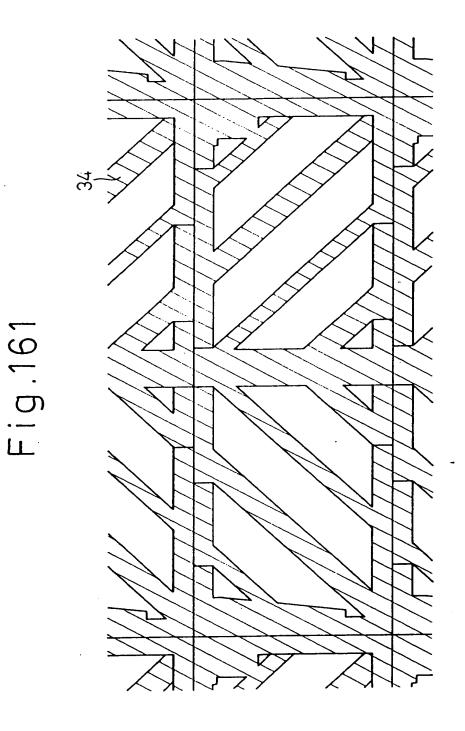




Fig.160



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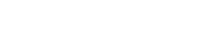


Fig.162

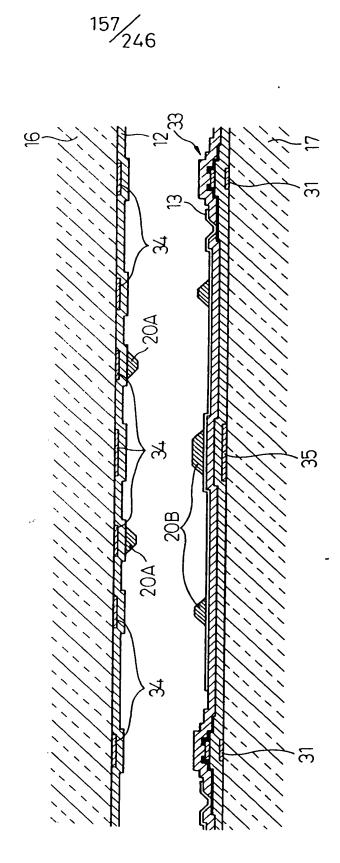
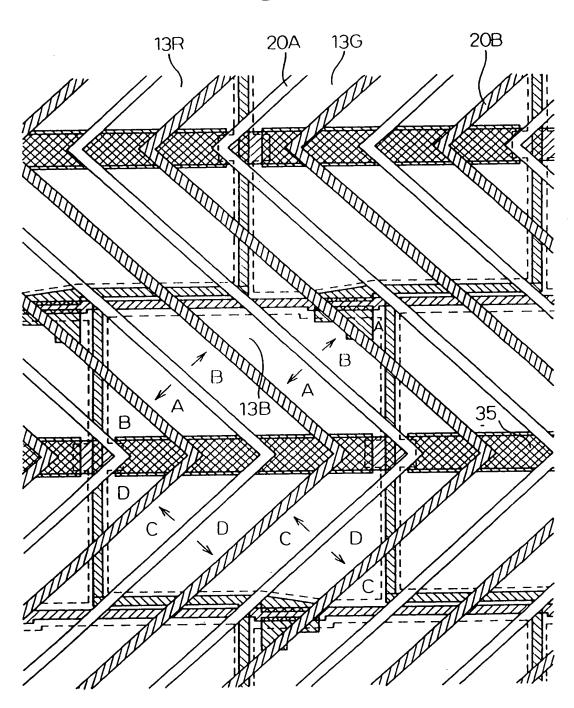
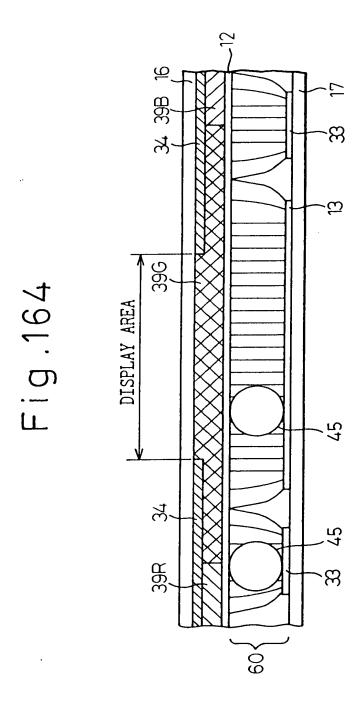


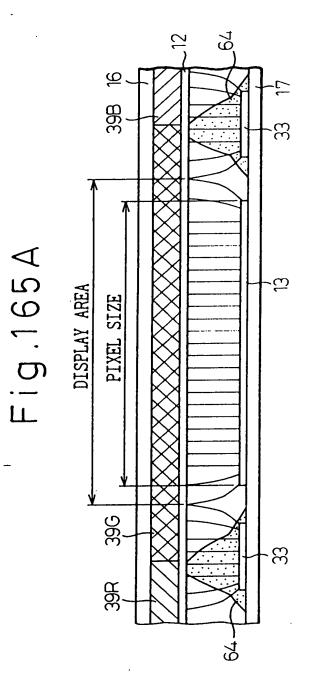


Fig.163





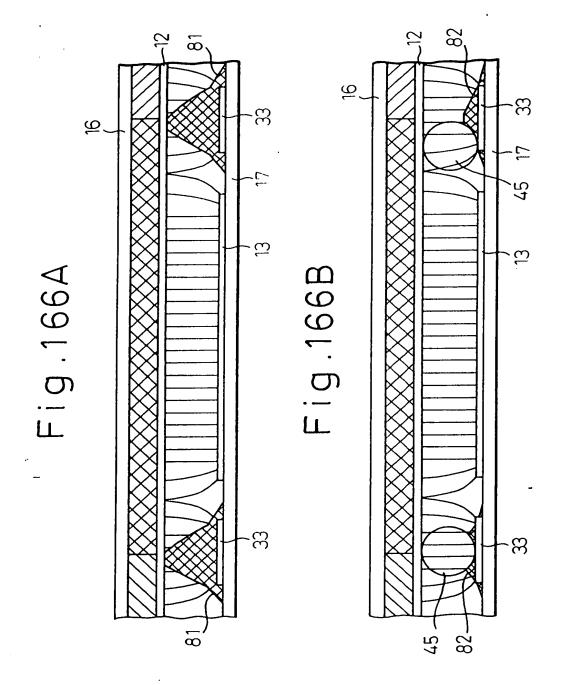
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8 9 Ж, 45 38B <u>À</u>, 39 13 45-

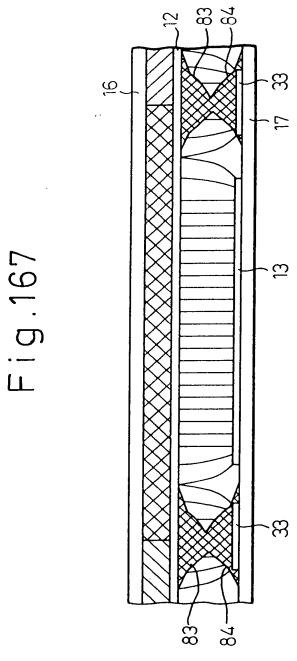
Fig.165B

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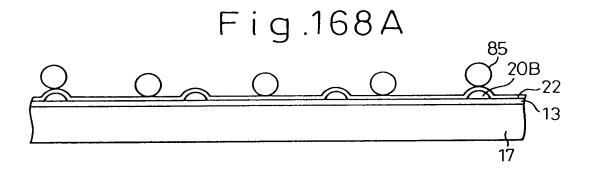


Fig.168B

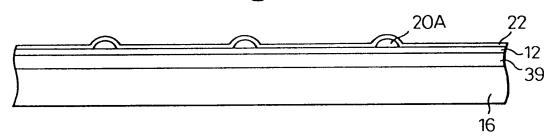
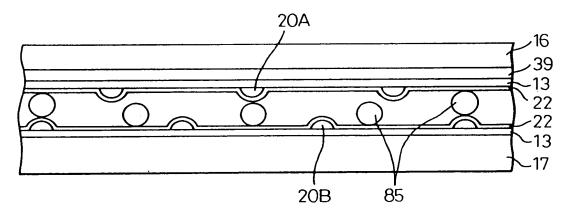
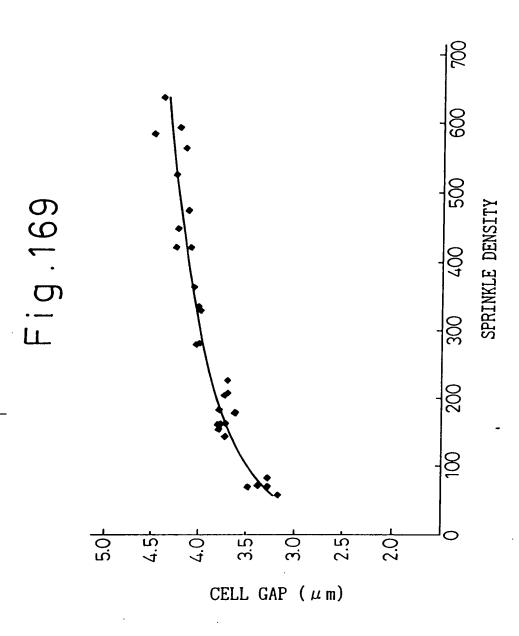


Fig.168C



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Fig.170

250	N	YES
200	ON	YES
057	NO	YES
007	NO	YES
350	9	YES
300	NO	NO.
250	NO	N N
200	NO	NO
150	NO	NO
100	YES	ON.
50	YES	NO
SPRINKLE DENSITY OF SPACERS (NUMBERS/mm²)	BLEMISH OCCURRENCE DUE TO PUSHING	BLEMISH OCCURRENCE DUE TO PULLING



Fig.171A

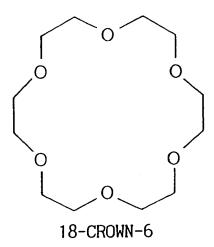


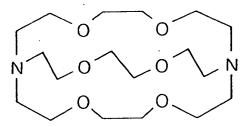
Fig.171B

DIBENZOYL-18-CROWN-6



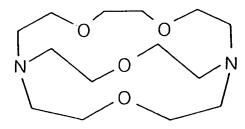
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Fig.172A



CRYPTAND [2.2.2]

Fig.172B



CRYPTAND [2.1.1]



Fig.173A

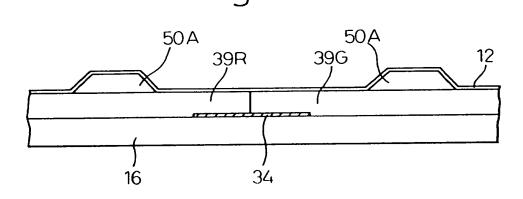


Fig.173B

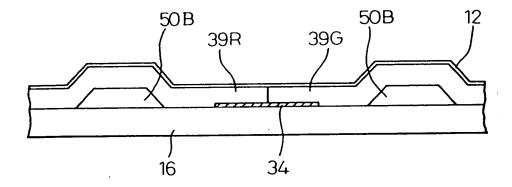




Fig.174

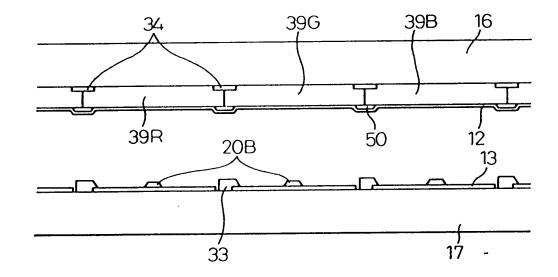




Fig.175A

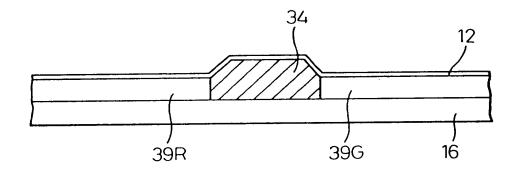


Fig.175B

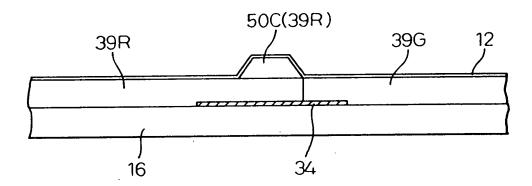




Fig.176A

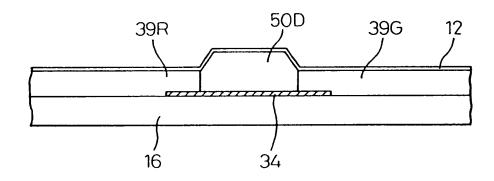


Fig.176B

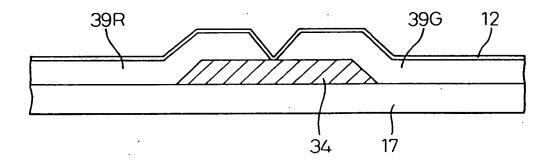




Fig.177A

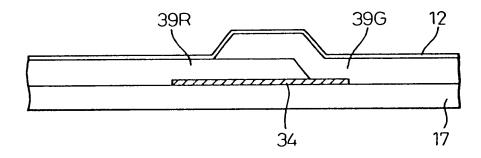
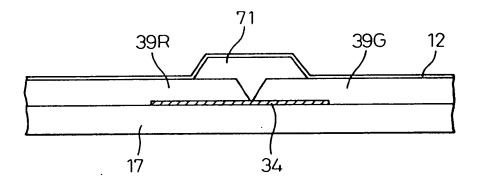
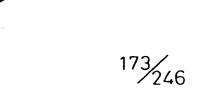


Fig.177B





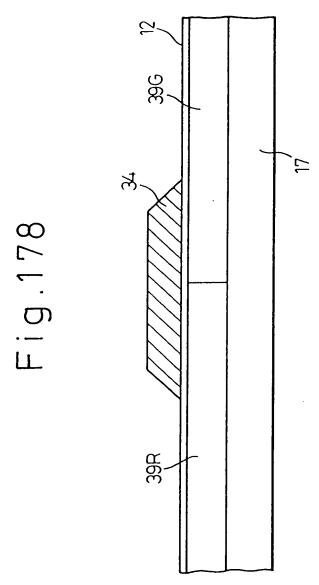




Fig.179A

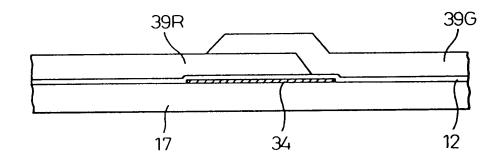


Fig.179B

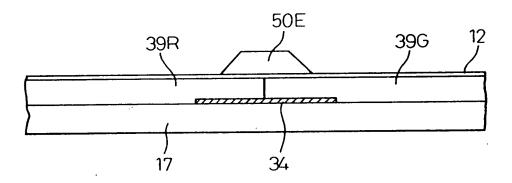




Fig.180A

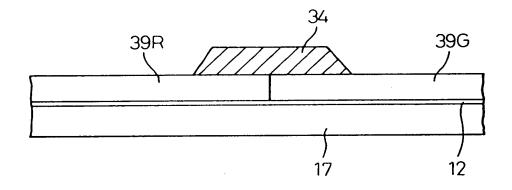
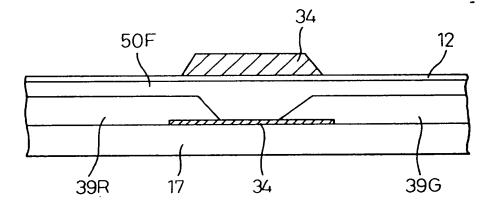
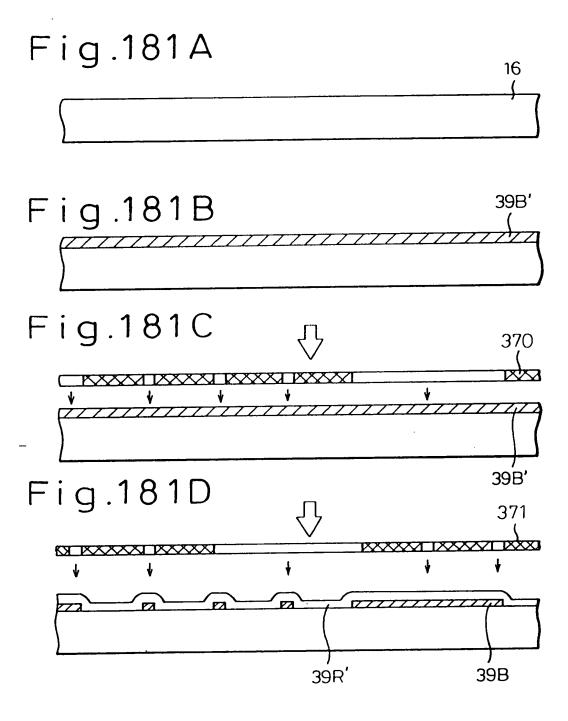


Fig.180B







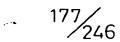


Fig.181E

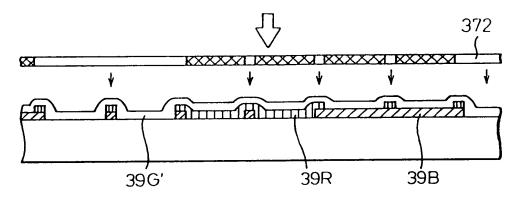


Fig.181F

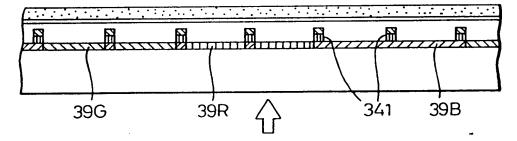


Fig.181G

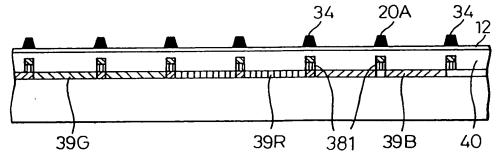
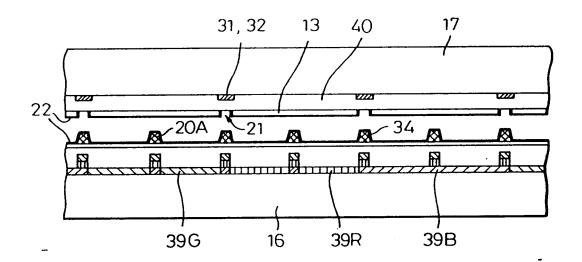
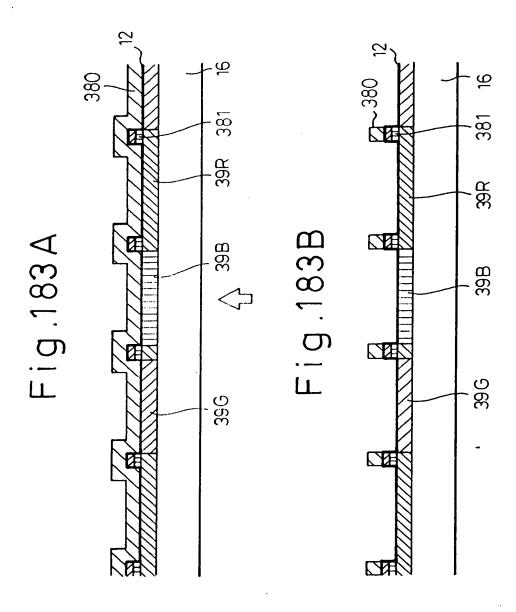




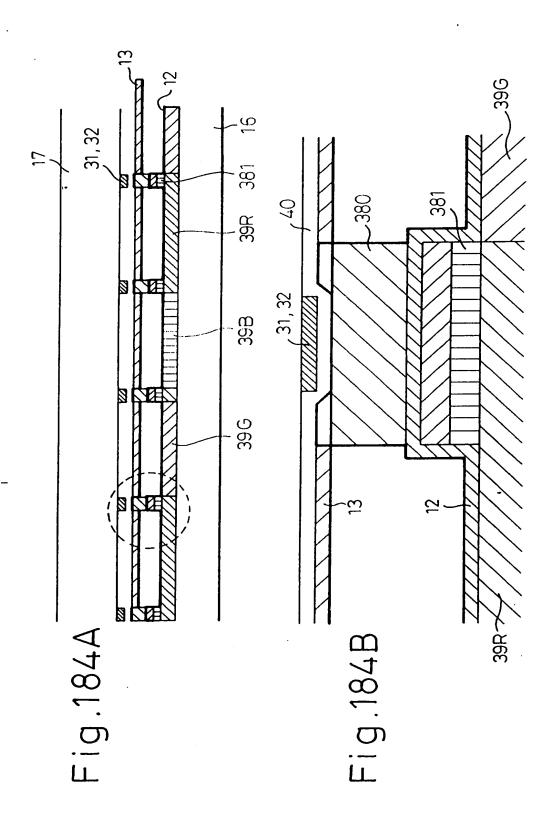
Fig.182



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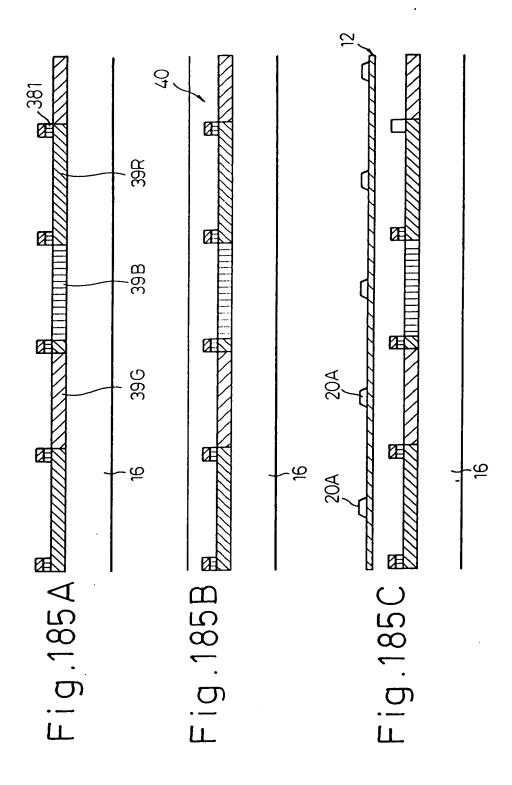








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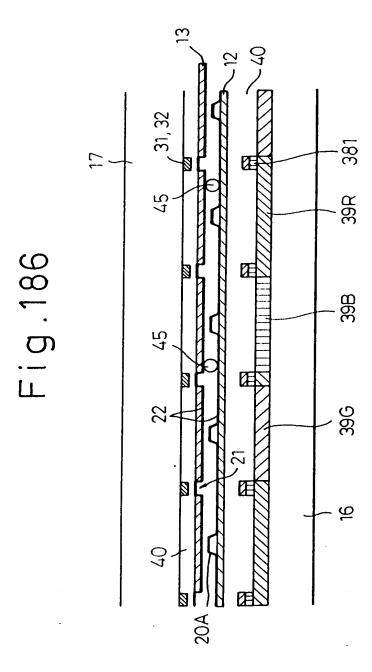
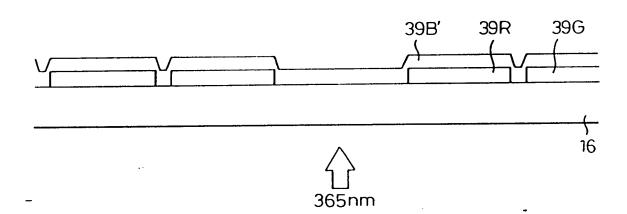


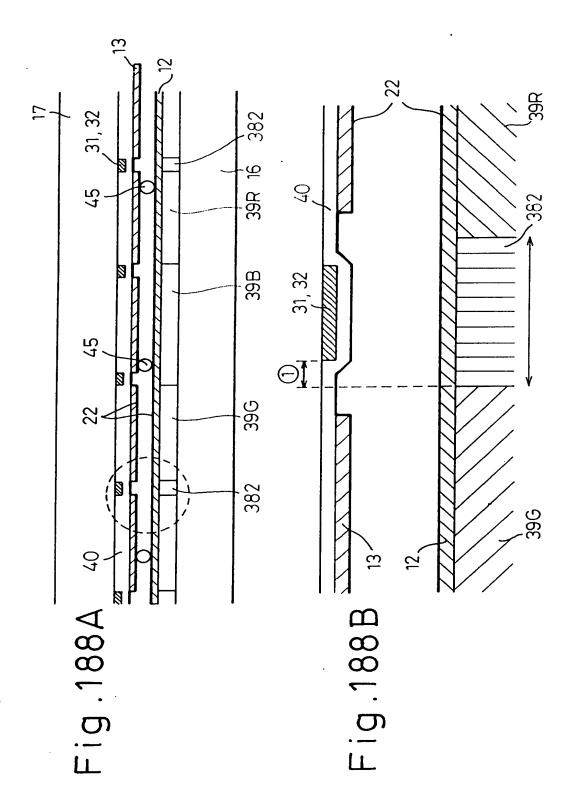


Fig.187





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Fig.189

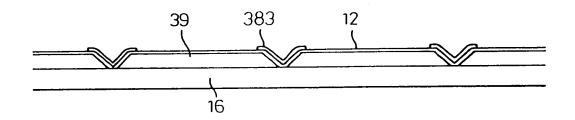


Fig.190A

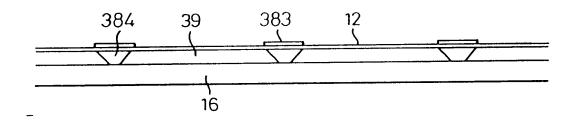


Fig.190B

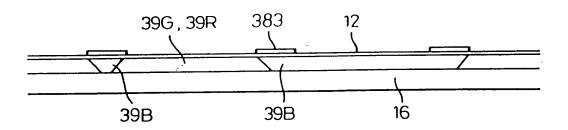




Fig.191

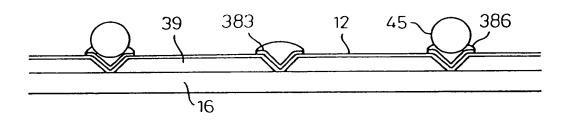


Fig.192

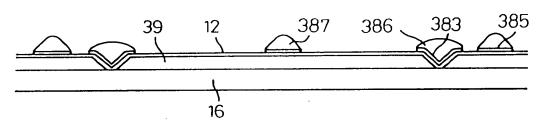


Fig.193

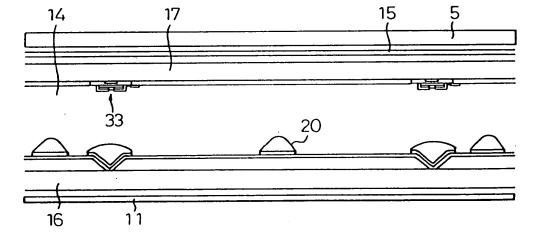




Fig.194

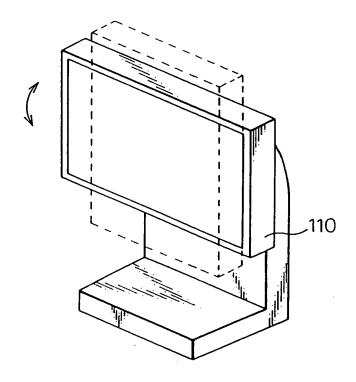


Fig. 195

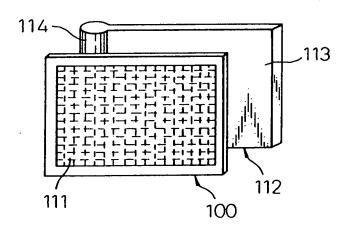




Fig.196A

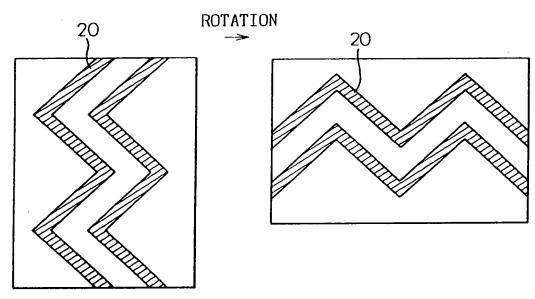


Fig.196B

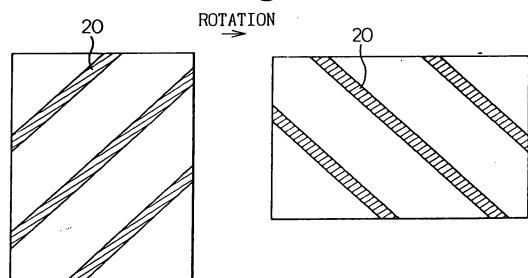




Fig.197

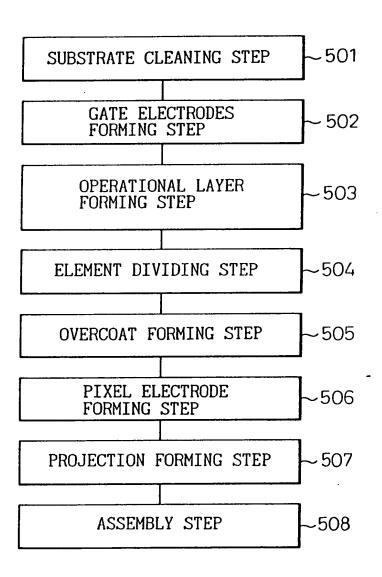




Fig.198

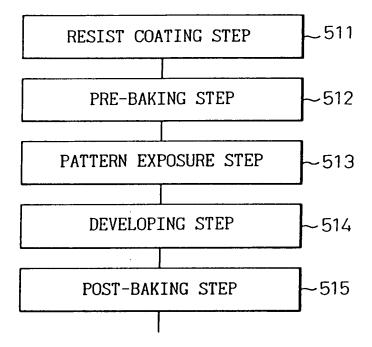
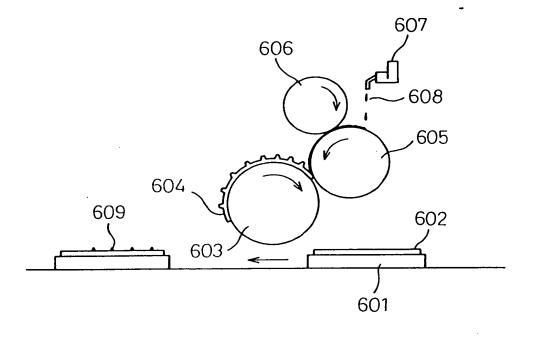


Fig.199



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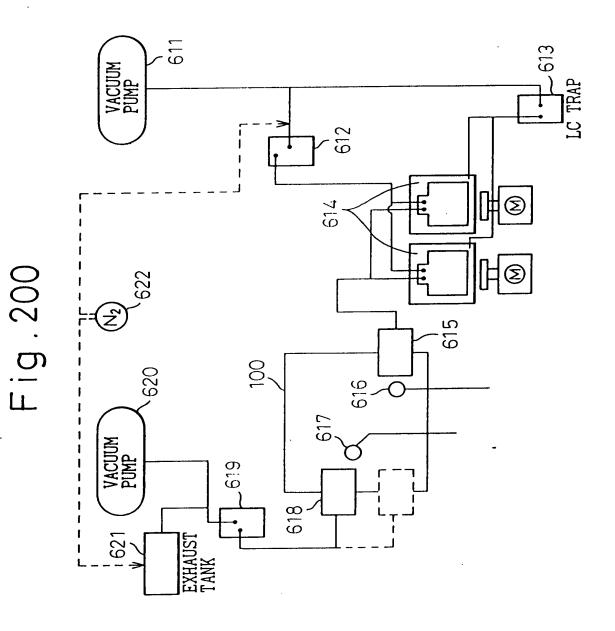




Fig. 201A

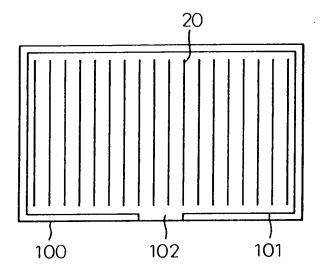
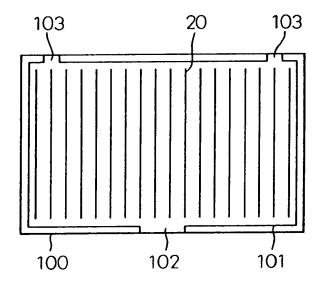


Fig.201B





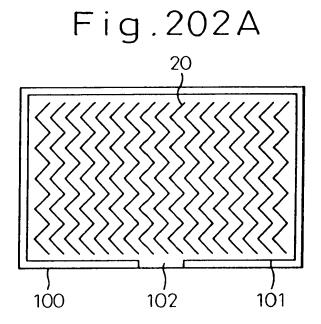


Fig.202B

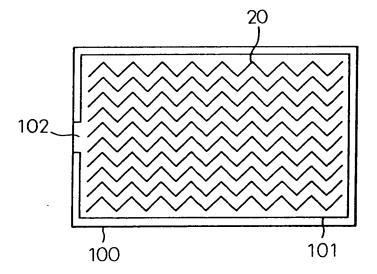




Fig. 203A

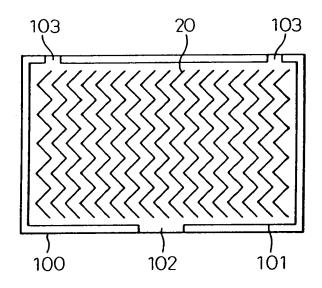


Fig.203B

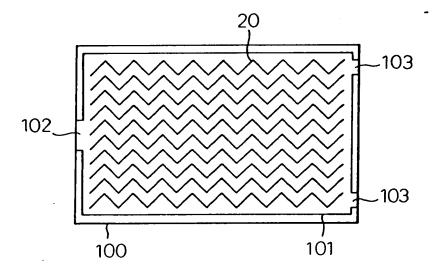
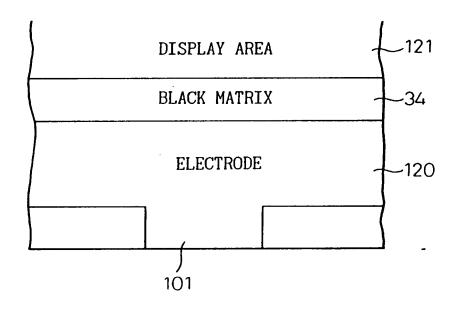




Fig. 204





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Fig.205A

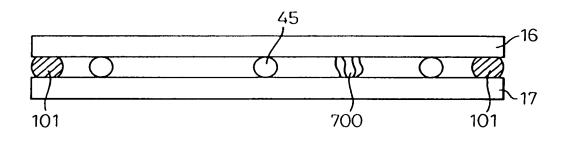
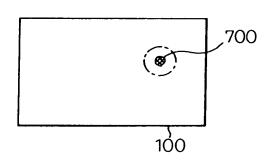


Fig.205B

Fig.205C



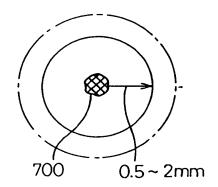
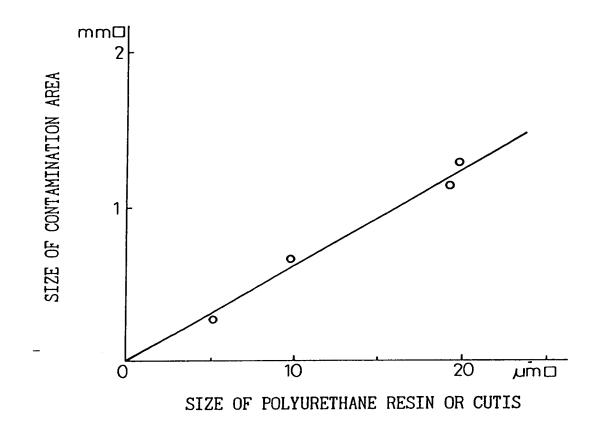
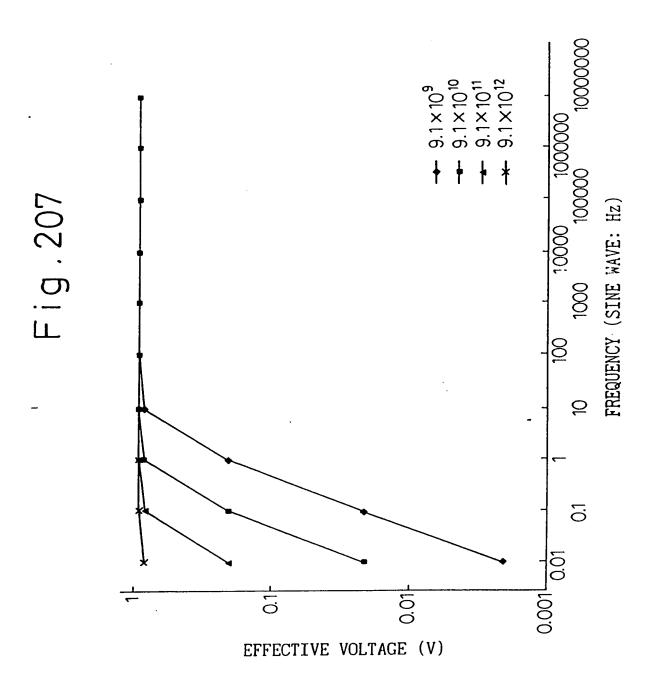


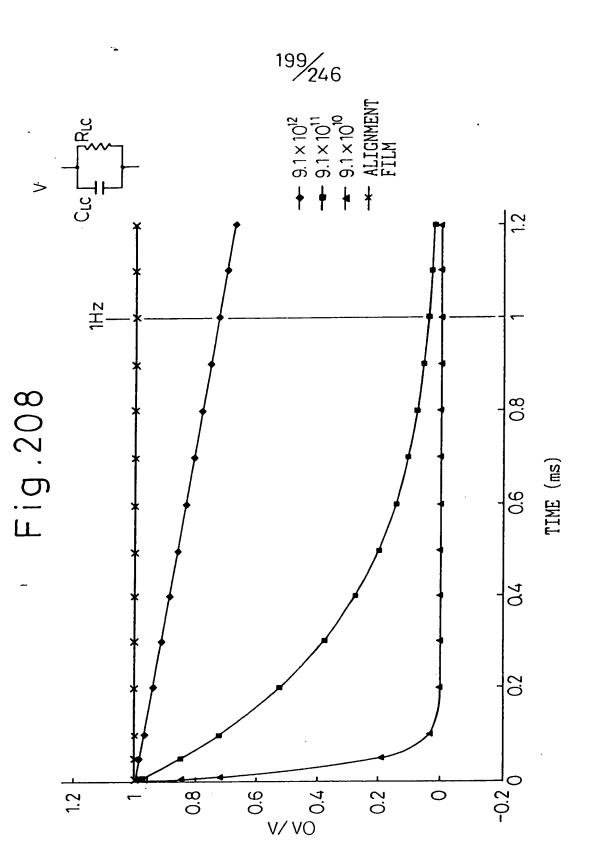


Fig.206



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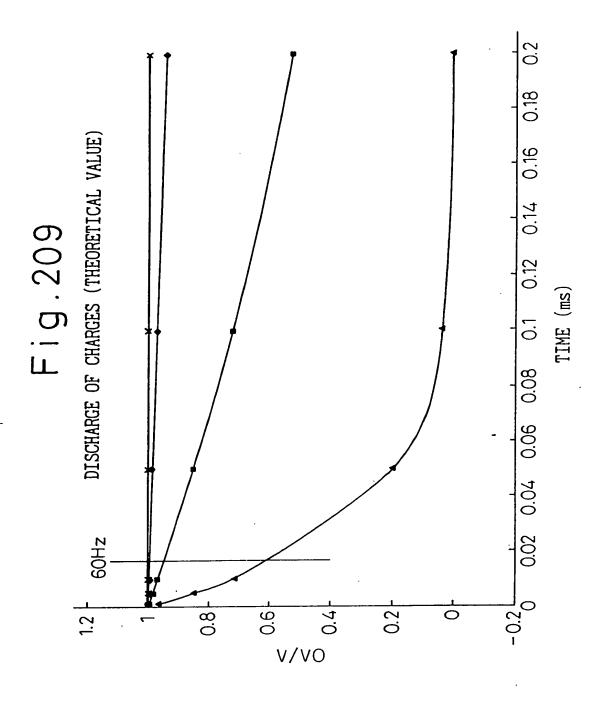




Fig.210

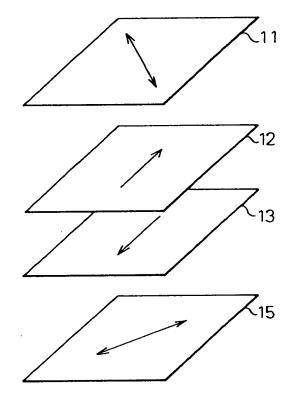




Fig.211

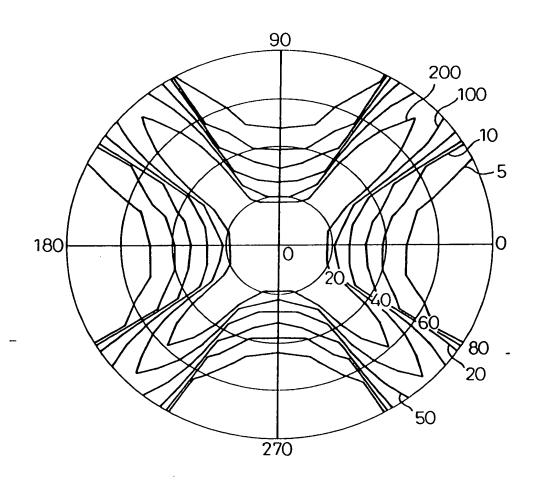




Fig.212

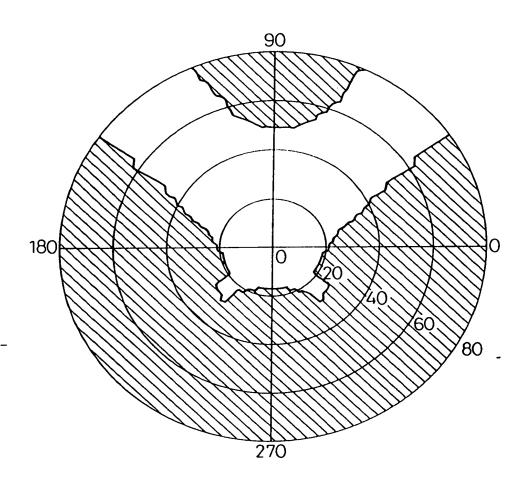






Fig.213

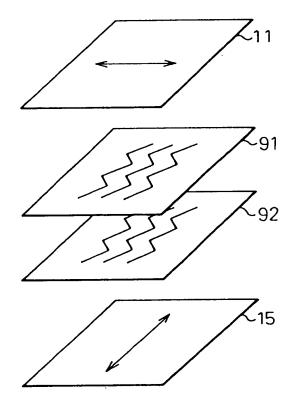




Fig. 214

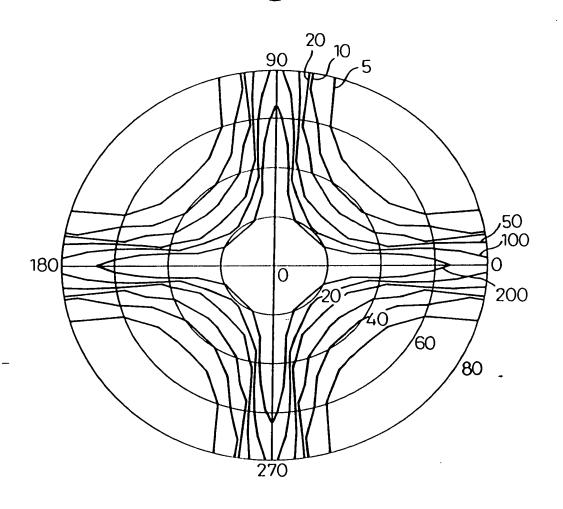




Fig.215

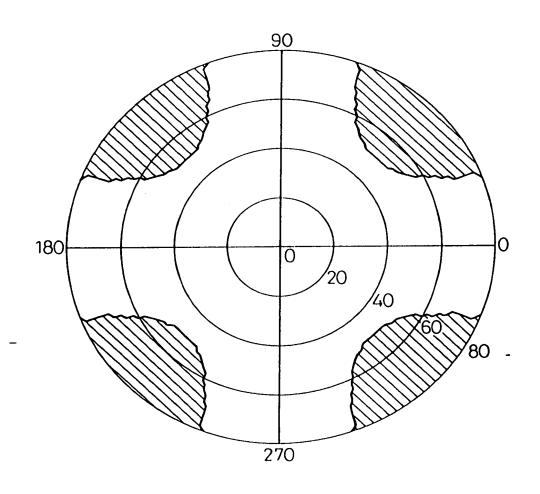
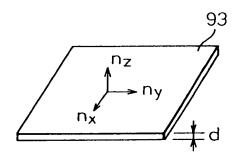




Fig.216



GENERAL CONDITION

 n_X , $n_Y \ge n_Z$

POSITIVE UNIAXIAL FILM

 $n_x > n_y = n_z$

NEGATIVE UNIAXIAL FILM

 $n_x = n_y > n_z$

BIAXIAL FILM (A PHASE LAG AXIS IS X DIRECTION.)

 $n_x > n_y > n_z$

RETARDATION IN INPLANE DIRECTIONS

 $R = (n_x - n_y)d -$

RETARDATION OF THICKNESS DIRECTION

 $R = \left(\frac{n_x + n_y}{2} - n_z\right) d$



Fig.217

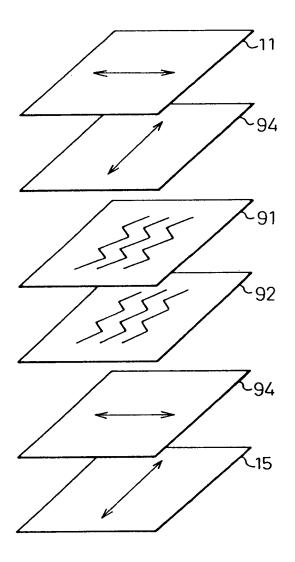




Fig.218

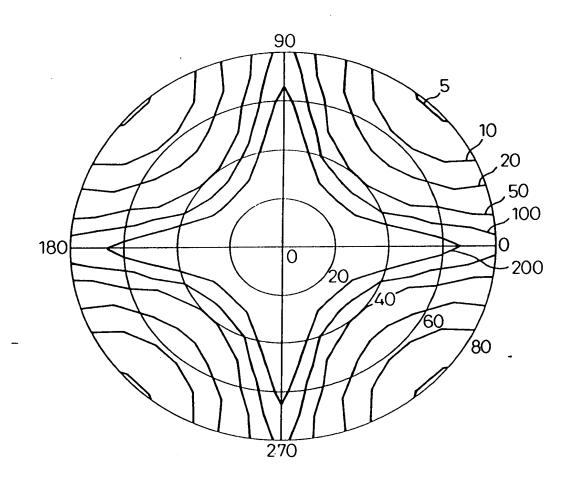
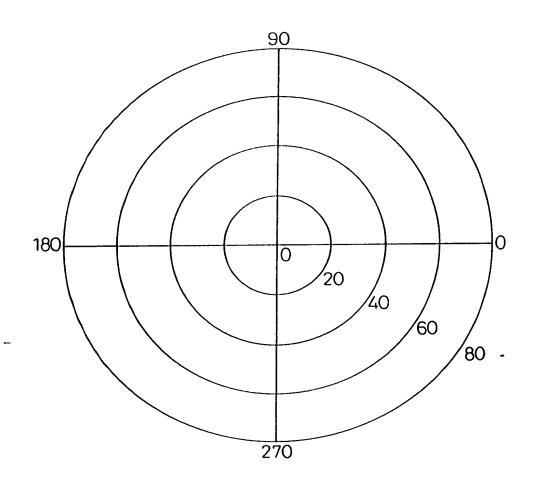




Fig.219





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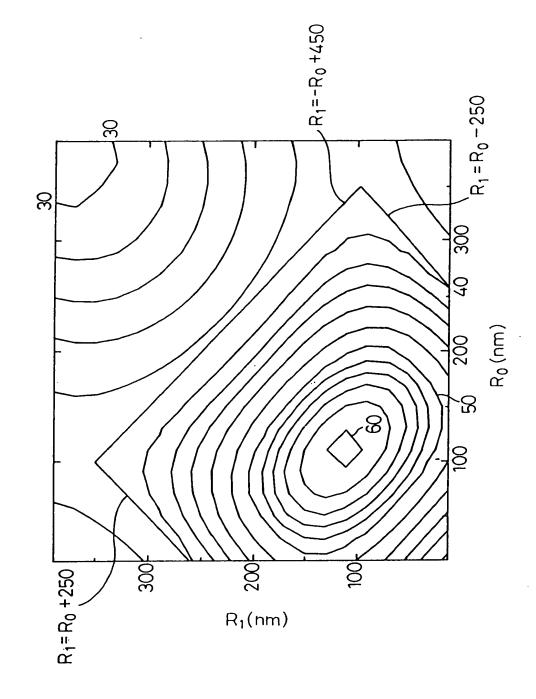


Fig.220



Fig. 221

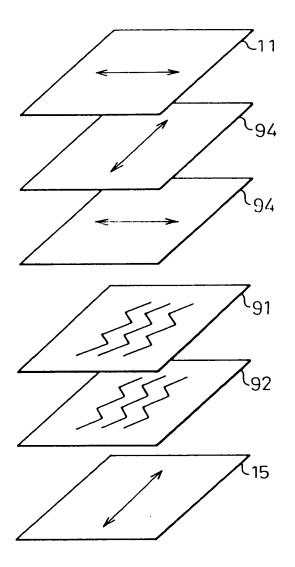




Fig. 222

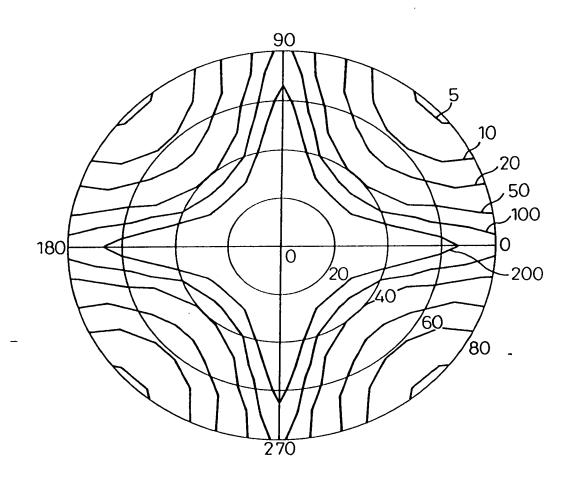




Fig.223

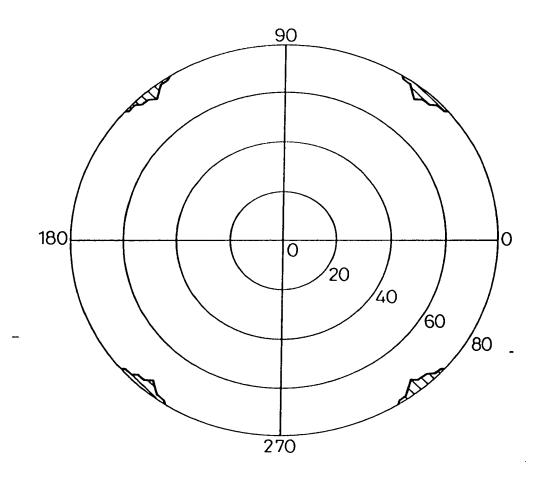




Fig.224

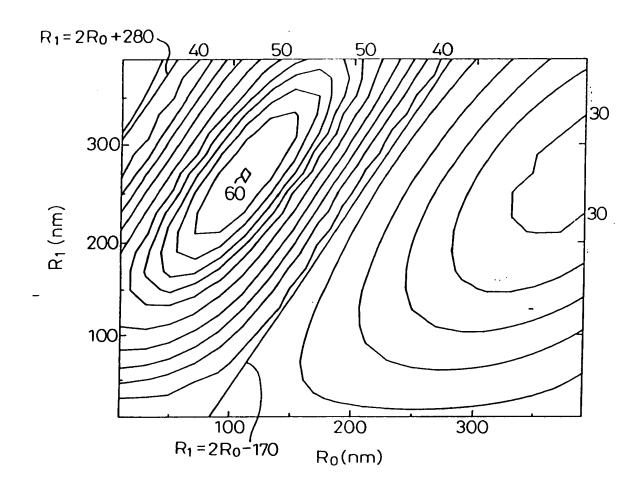




Fig.225

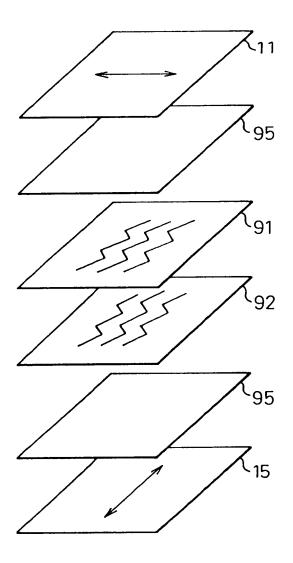




Fig. 226

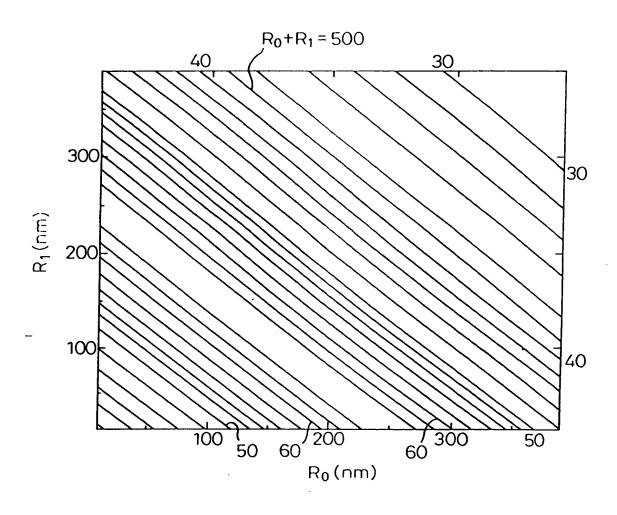




Fig.227

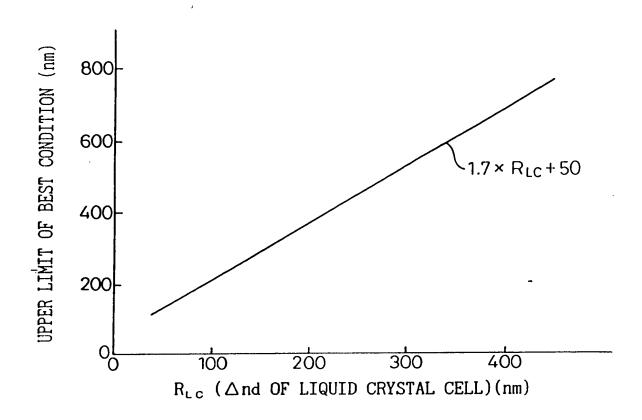




Fig.228

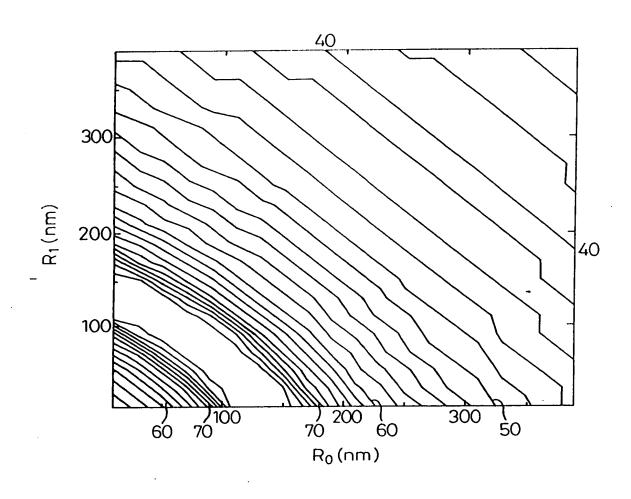




Fig.229

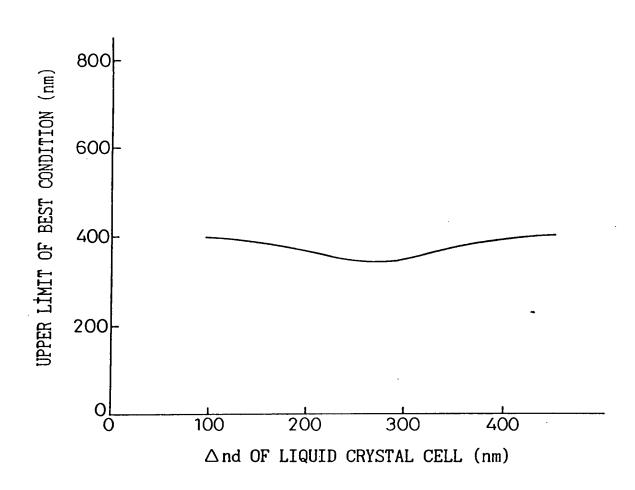




Fig.230

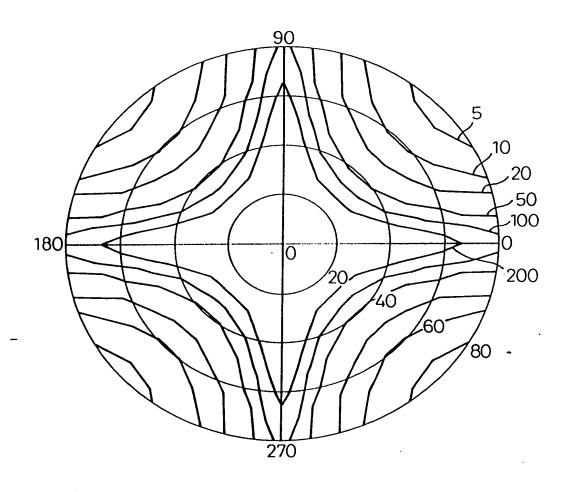




Fig. 231

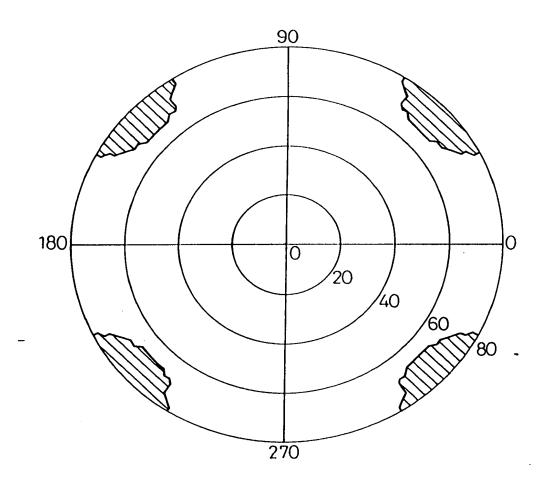




Fig.232

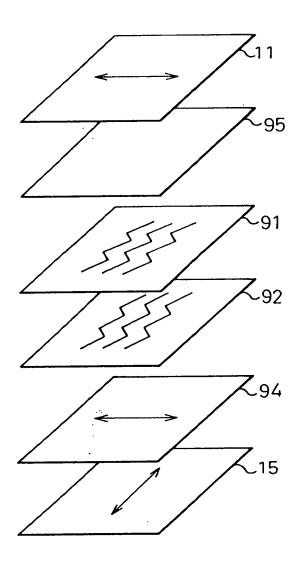


Fig.233

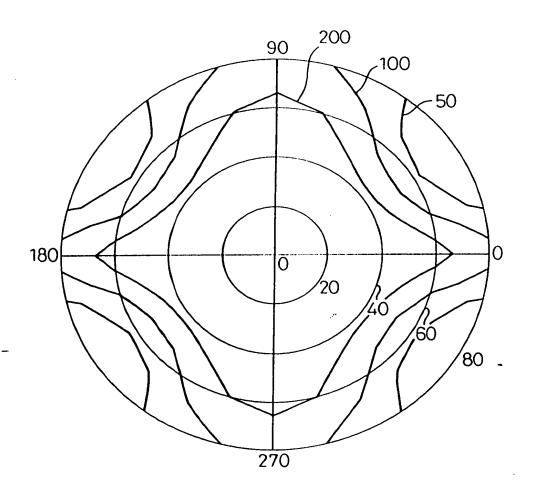




Fig. 234

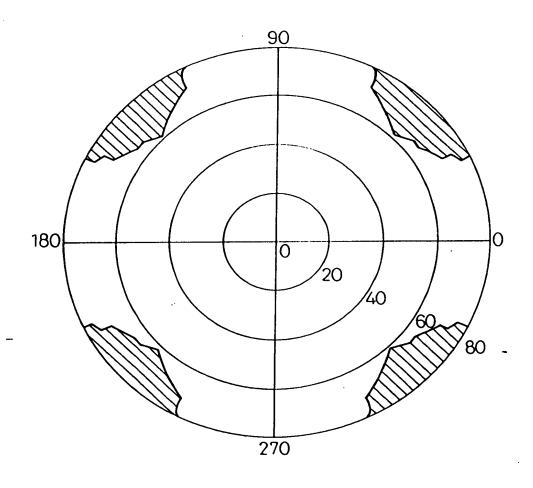




Fig. 235

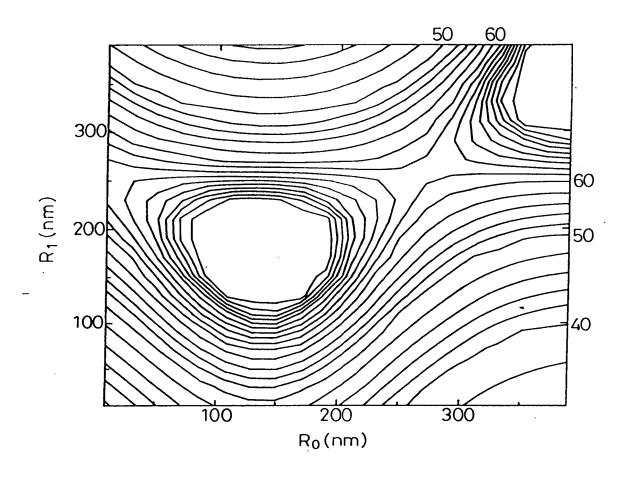




Fig.236

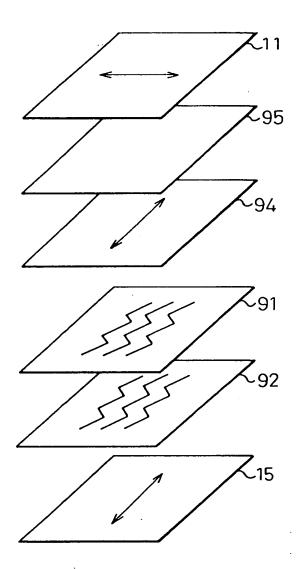






Fig.237

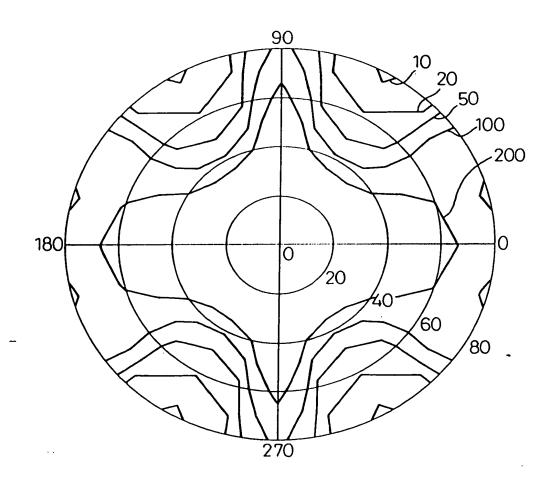




Fig.238

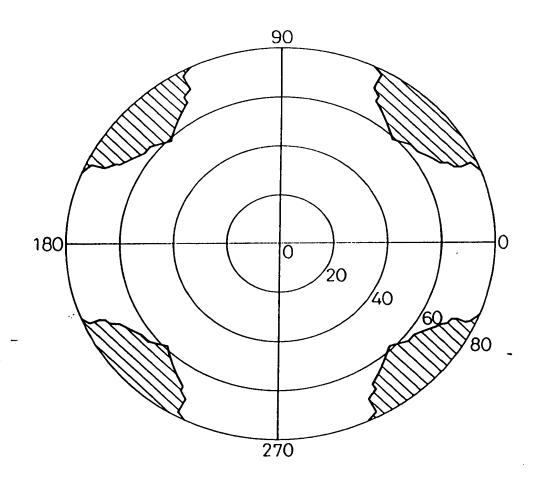




Fig.239

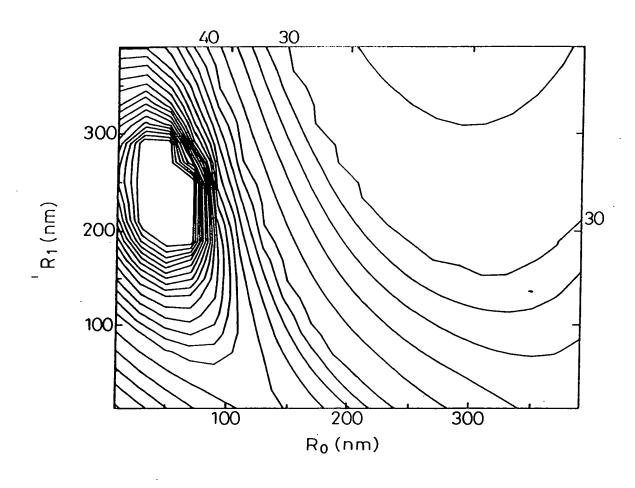
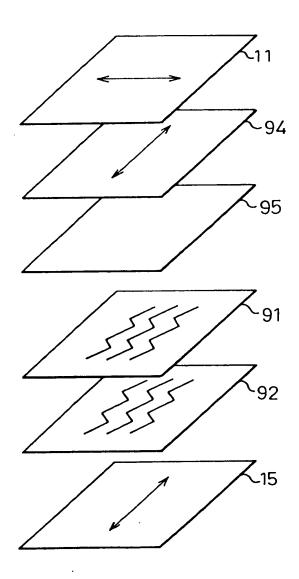






Fig. 240



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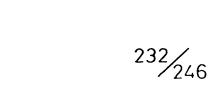


Fig.241

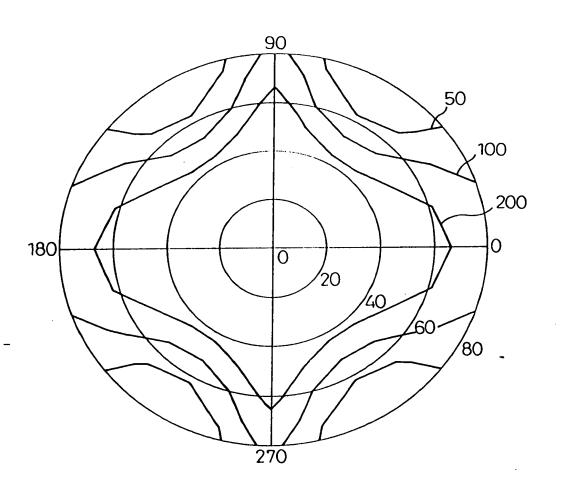




Fig. 242

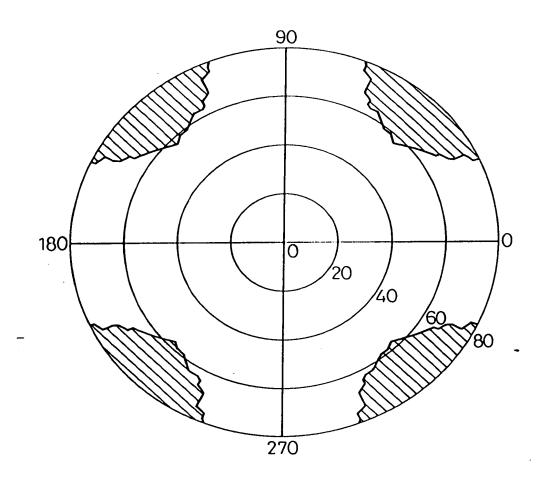




Fig.243

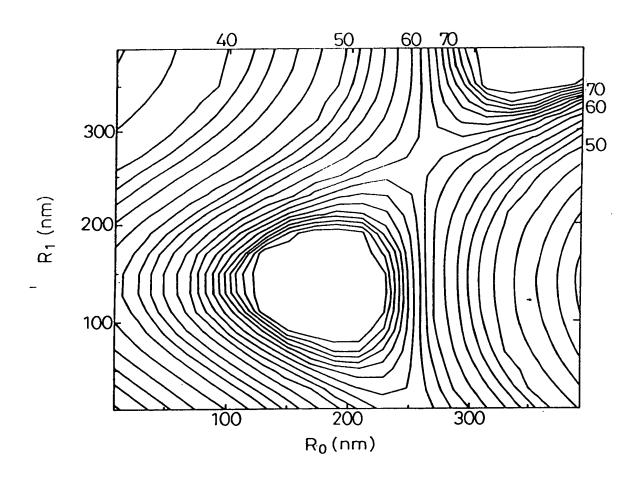




Fig. 244

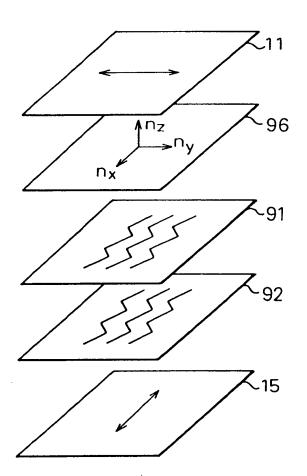




Fig.245

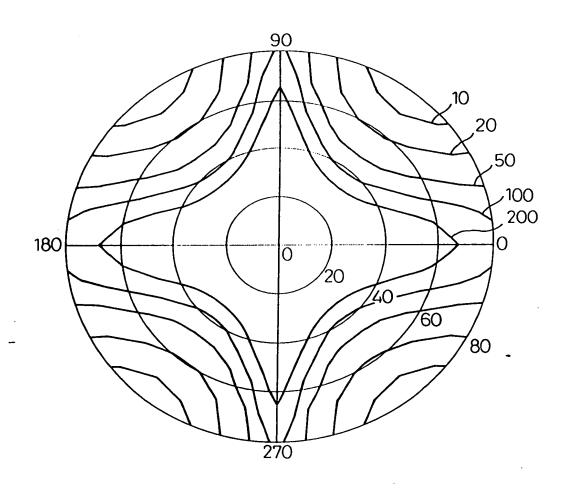
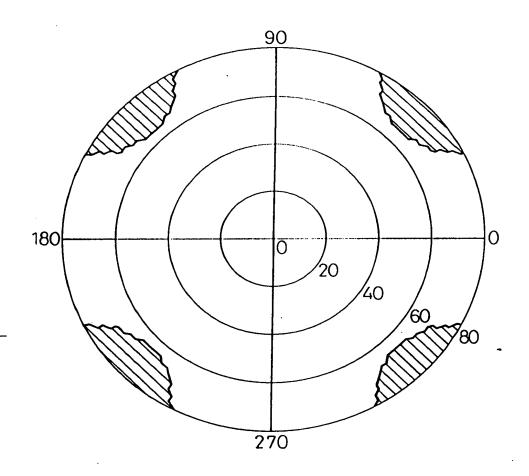




Fig. 246







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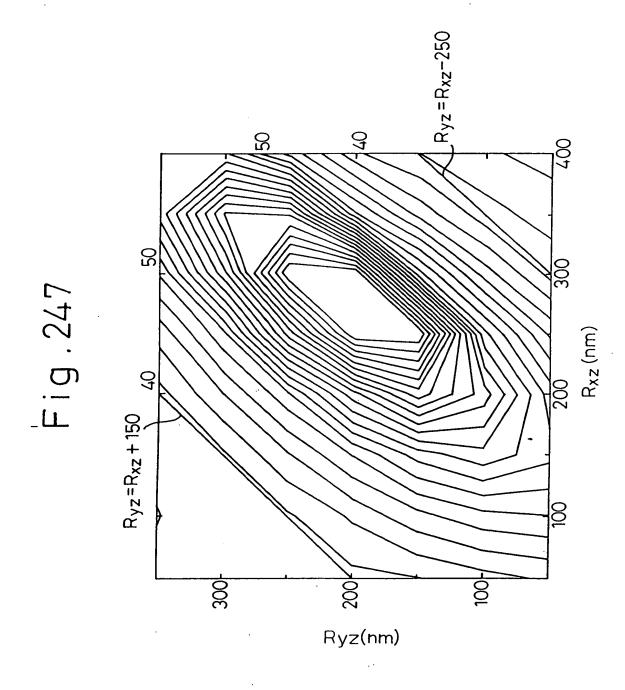
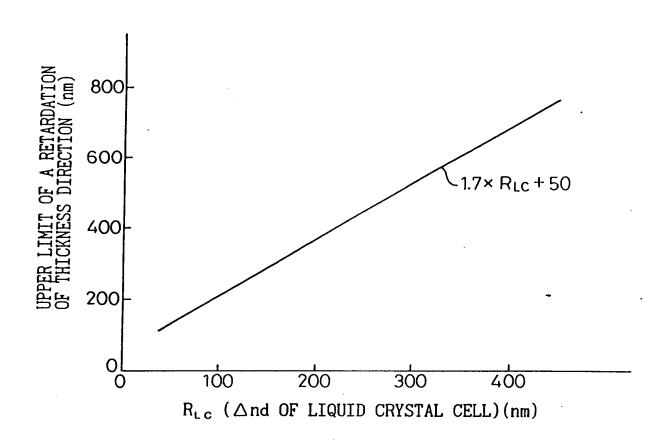




Fig.248



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		,						
DIFFERENCE: LEFT)	Δv(Y)		0.03	0.05		0.02	0.12	
COLOR (5v	\(\x\)\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		0.03	0.03		90.0	0.14	
VIEW ANGLE : CR > 10	LEFT-RIGHT DIRECTION		.08+1	°08+1		。 0 +1	÷ 80°	
TRANS- MITTANCE	(26)		5.60	5.60		4.50	5.80	
PHASE DIFFERENCE FILM	Rd VALUE (nm)		320	320		240	320	
P BETWI OJECTI((µ m)	ם ט צ		20, 25, 30	20, 25, 30	(H, G, B=30	R,G,B=30	
THICKNESS OF A PANEL (m m)	מ ס צ		5.7, 4.6, 3.6	EMBODIMENT 5.7, 4.6, 3.6	(((7, G, B=3.0	PRIOR ART R,G,B=4.6	
SAMPLE		FMRODIMENT	A	EMBODIMENT B	TAM ADTAG	1 1 1	PRIOR ART	,

Fig. 249



Fig. 250

EXAMPLES	INITIAL VALUES	AFTER 200 HOURS
EMBODIMENT C	25	42
EMBODIMENT D	33	51
EMBODIMENT E	26	45
EMBODIMENT F	30	48
REFERENCE	32	70



Fig.251A

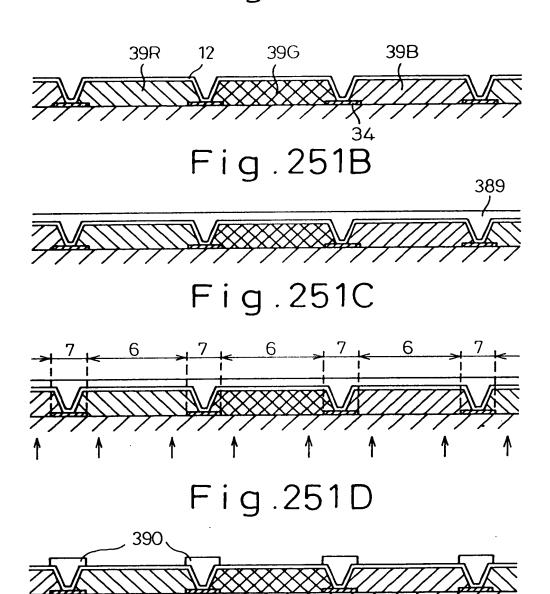




Fig.252A

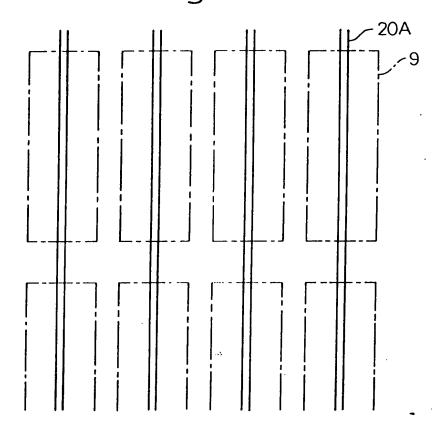


Fig.252B

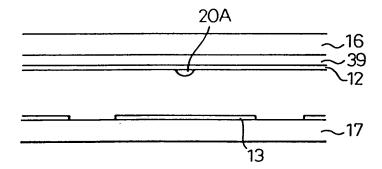
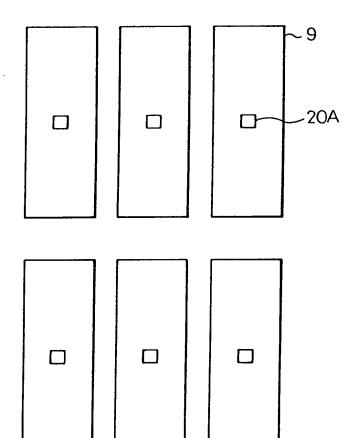






Fig. 253





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Fig.254A

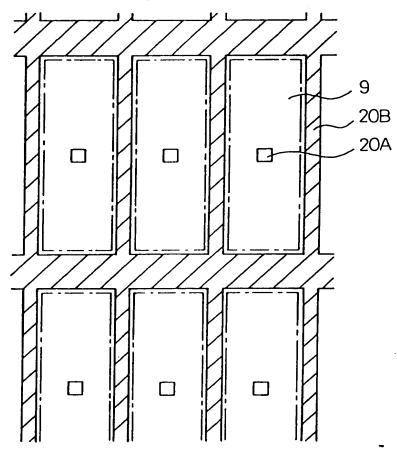
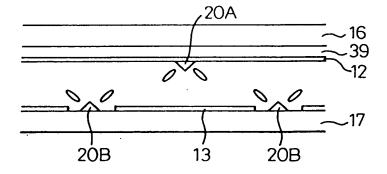


Fig.254B







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Fig.255

